

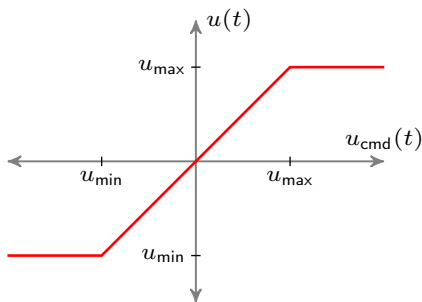
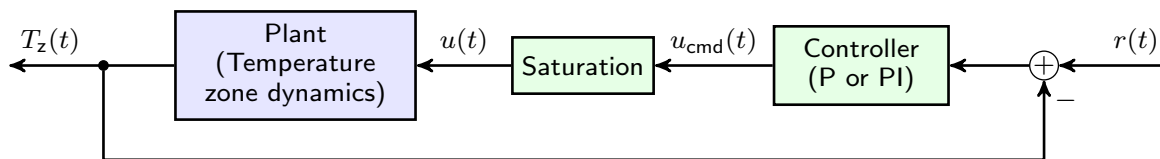
# Building control

## Lecture 5: Saturation, relay control and discretization

Roy Smith

### Saturation

#### Plant actuation limitations



$$u(t) = \begin{cases} u_{\max} & \text{if } u_{\text{cmd}}(t) > u_{\max} \\ u_{\text{cmd}}(t) & \text{if } u_{\min} \leq u_{\text{cmd}}(t) \leq u_{\max} \\ u_{\min} & \text{if } u_{\text{cmd}}(t) < u_{\min} \end{cases}$$

## Saturation

### Plant actuation effects

When the input is saturated (e.g.  $u_{\text{cmd}}(t) > u_{\text{max}}$ ) then the interconnection is of the plant and controller is non-linear.

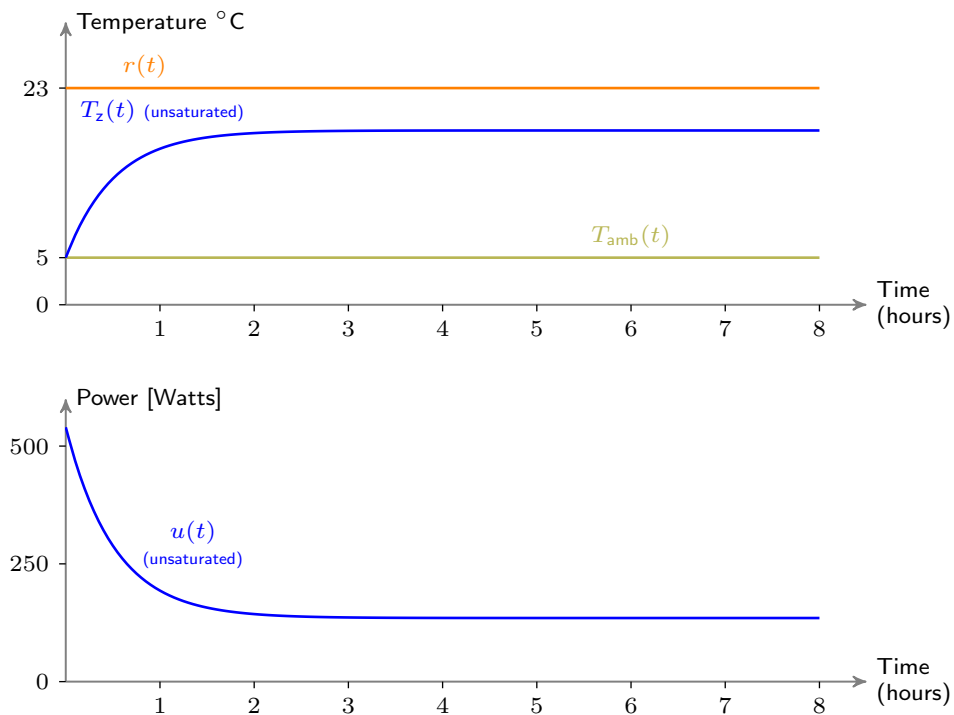
For small changes in the disturbance or the reference, the input to the plant will not change.

### Cost efficient actuation

Many building systems operate with their actuators in saturation due to capital equipment cost constraints.

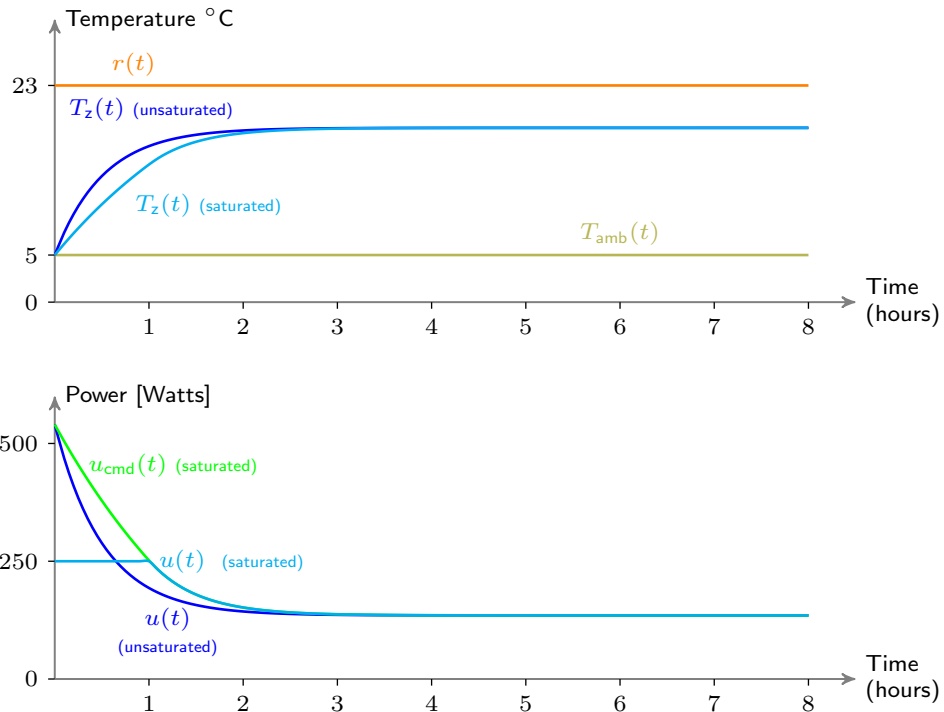
## P-control, unsaturated input

$$K_P = 30$$



## P-control, saturated input

$$K_P = 30, \quad u_{\min} = 0W, \quad u_{\max} = 250W$$

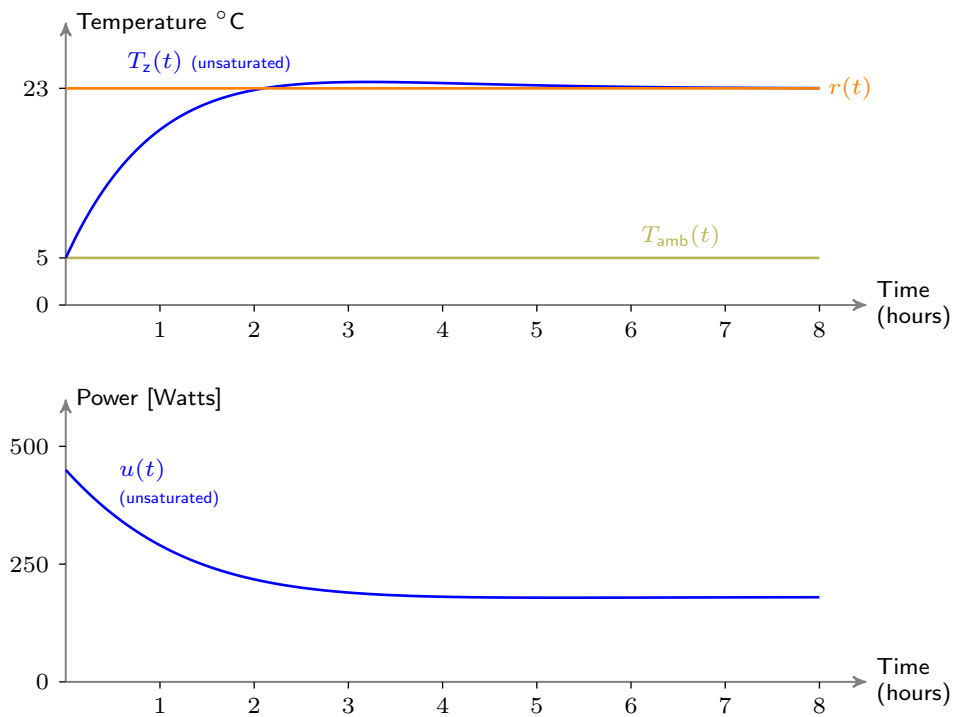


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## PI-control, unsaturated input

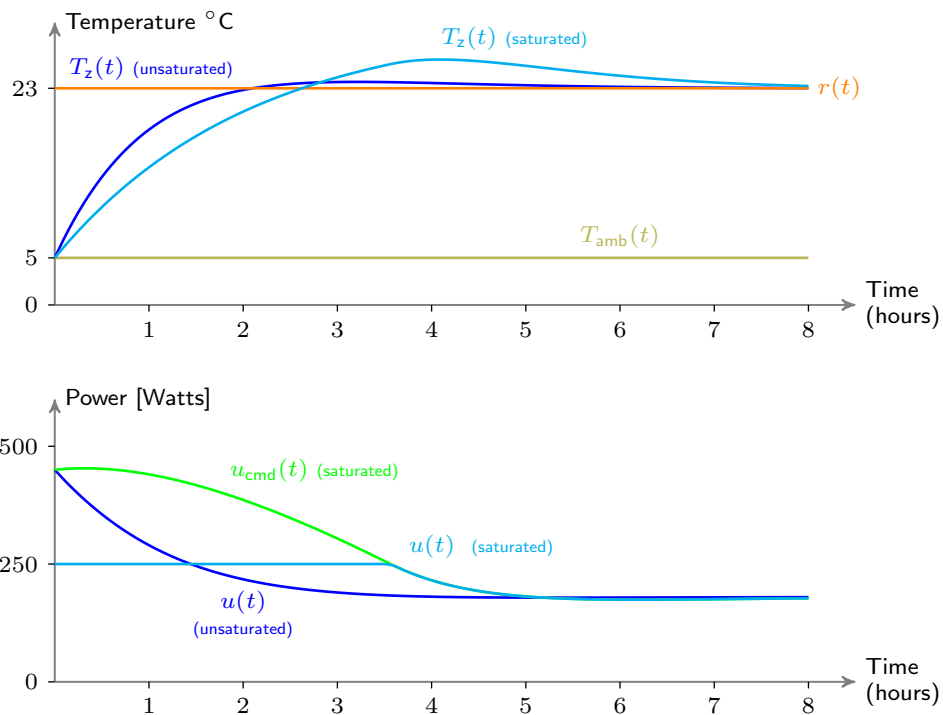
$$K_P = 25, \quad K_I = 0.005$$



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## PI-control, saturated input



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## Saturation

### Integrator windup

PI controller:

$$u(t) = K_P e(t) + K_I \int_0^t e(t) dt.$$

Saturation has the effect of keeping  $e(t)$  larger than it would have otherwise been.

The integrator continues to integrate an error that the controller cannot easily reduce (“windup”).

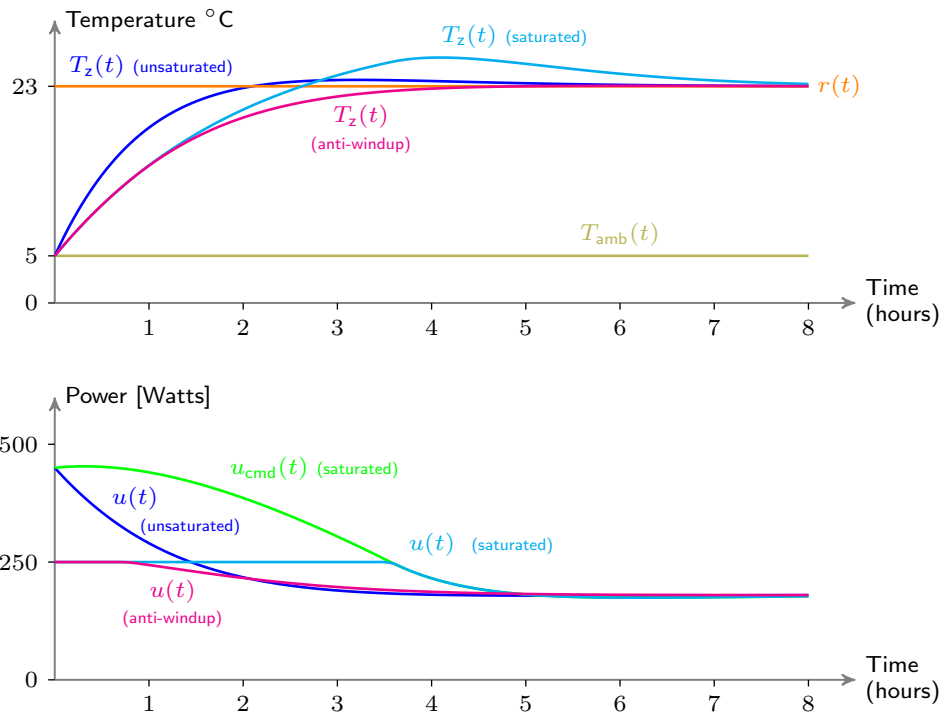
So  $u(t)$  becomes larger than it should,

and we have to have error in the opposite direction (overshoot) to bring the integrator back down to its correct level.

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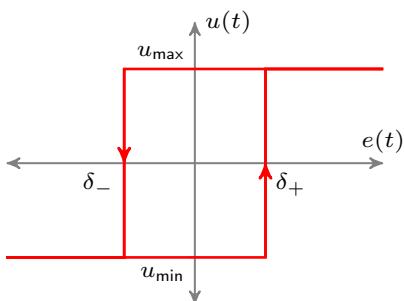
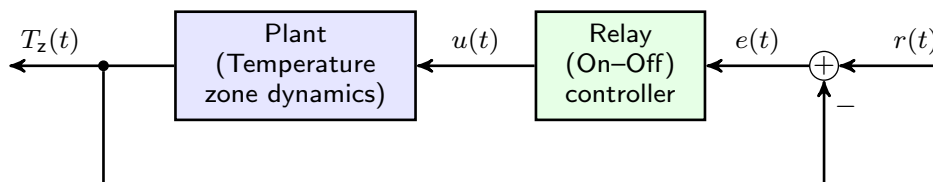
## PI-control with anti-windup compensation



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## Relay control (with hysteresis)



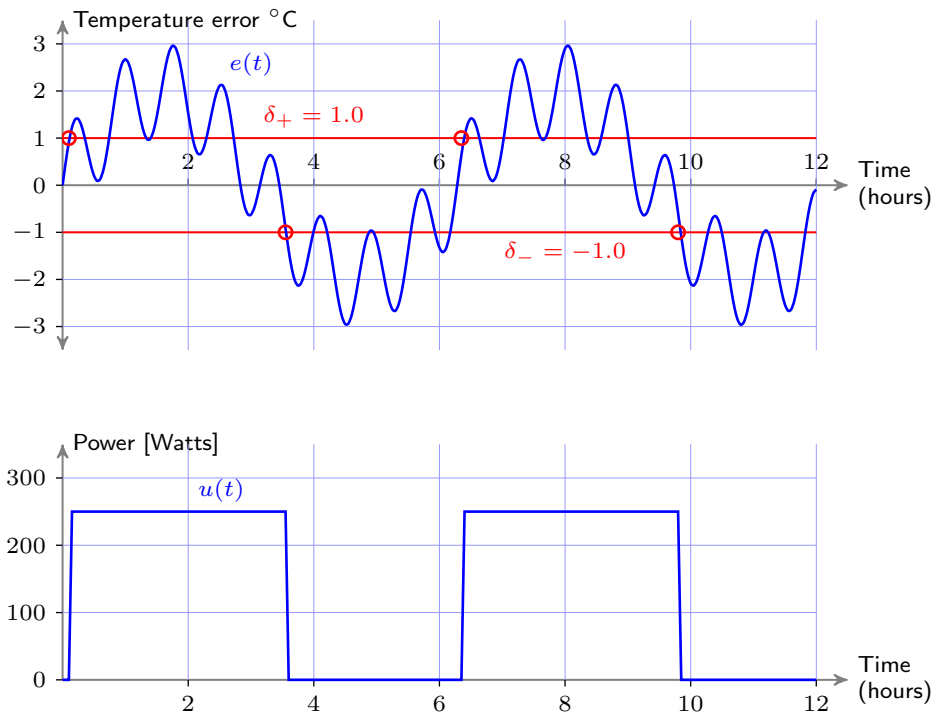
### Switching rules

- ▶ If  $u(t) = u_{\min}$  and  $e(t) \geq \delta_+$ ,  
then  $u(t) = u_{\max}$ .
- ▶ If  $u(t) = u_{\max}$  and  $e(t) \leq \delta_-$ ,  
then  $u(t) = u_{\min}$ .

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## Relay actuator

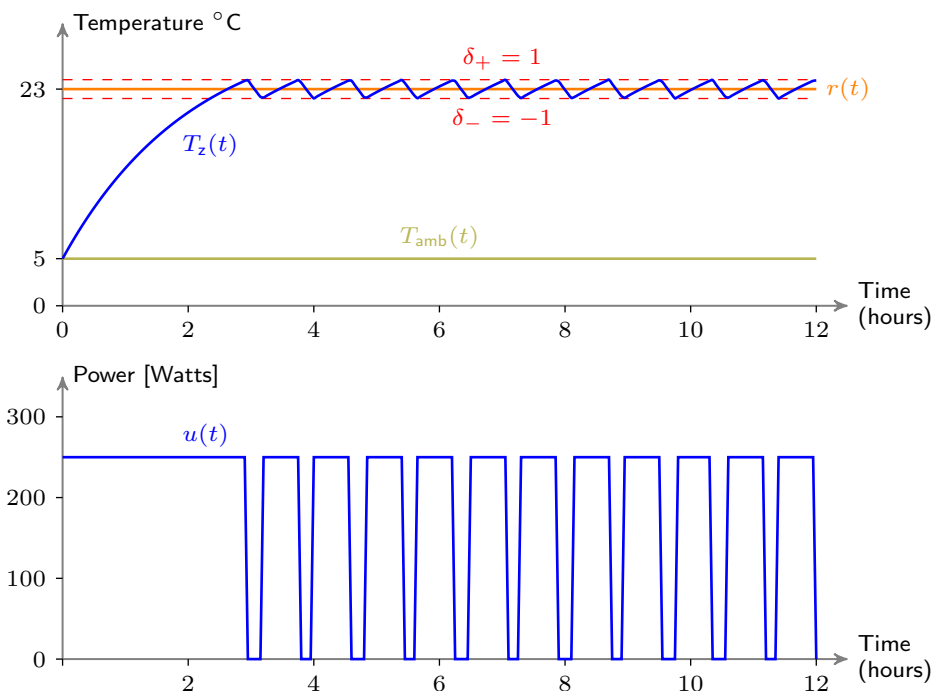


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## Relay control

### Reference tracking

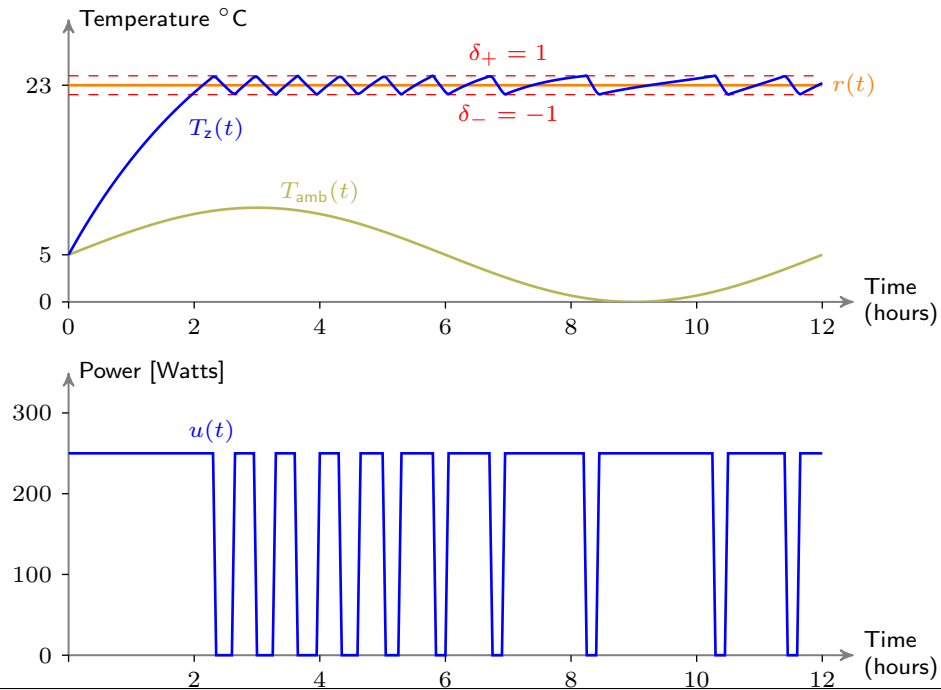


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## Relay control

### Disturbance rejection



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## Relay control

### Common building applications

- ▶ Thermostatic control:
  - ▶ Room temperature (heating, air-conditioning);
  - ▶ Refrigeration;
  - ▶ Water heaters.
- ▶ Fans (chillers, ventilation systems).
- ▶ Simple gas burners.

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## Digital controllers

### Why use digital controllers?

- ▶ Easily reprogrammed or modified.
- ▶ Complex algorithms (or optimisations) can be implemented.
- ▶ Integration with remote systems (via internet).

## Digital controllers

### Why use digital controllers?

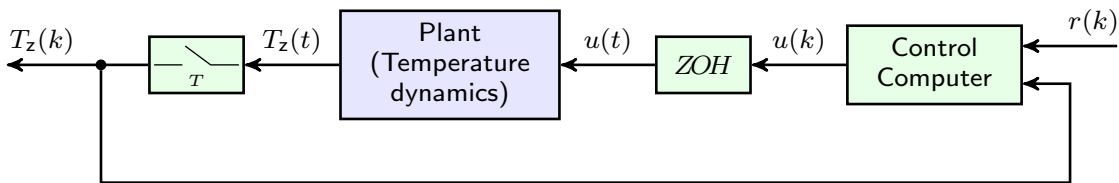
- ▶ Easily reprogrammed or modified.
- ▶ Complex algorithms (or optimisations) can be implemented.
- ▶ Integration with remote systems (via internet).

### Why use analogue controllers?

- ▶ Simple and low cost in mass production.
- ▶ Highly reliable.



## Digital controllers in a feedback loop



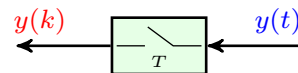
### Components:

- ▶ Plant: continuous-time thermal dynamics;
- ▶ Controller: discrete-time control calculations
- ▶ Sampler (A/D converter). Measures  $T_z(t)$  every  $T$  seconds;
- ▶ Zero-order hold (D/A converter): “holds” the value of  $u(k)$  for  $T$  seconds.

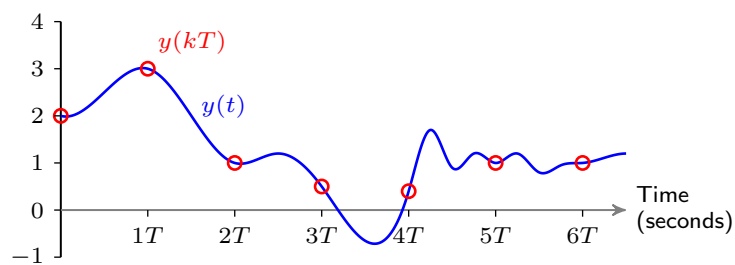
## Components: sampler

$$y(k) = y(t) |_{t=kT}, k = 0, 1, 2, \dots$$

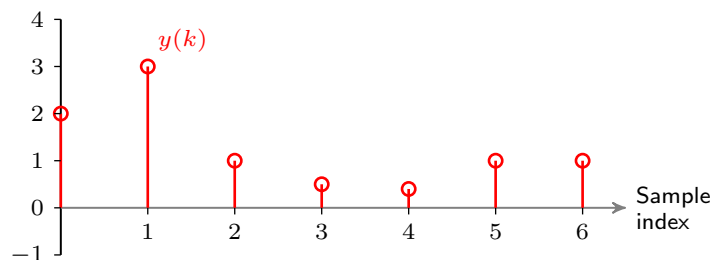
$T$  is the sampling period.



Continuous signal:

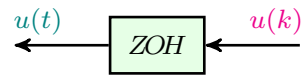


Discrete sequence:

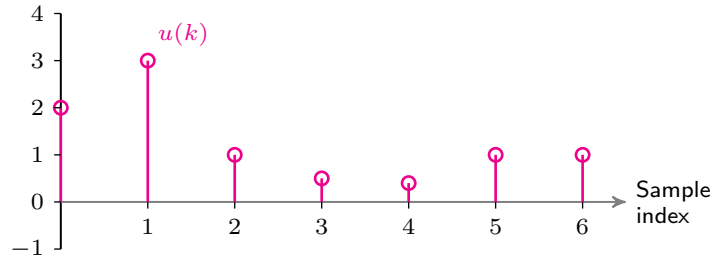


## Components: zero-order hold

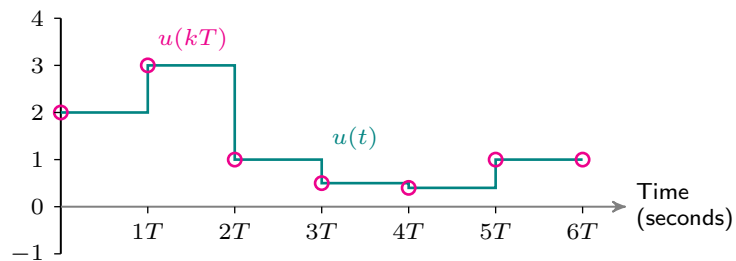
$$u(t) = u(k), \quad \text{for } kT \leq t < kT + T.$$



Discrete sequence:

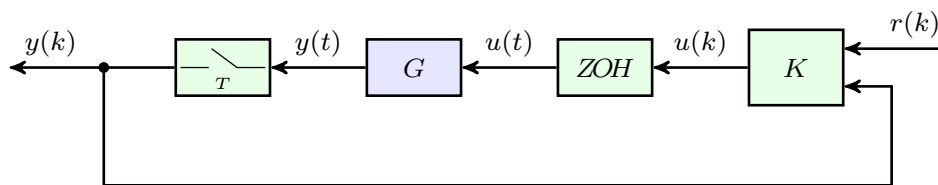


Continuous signal:

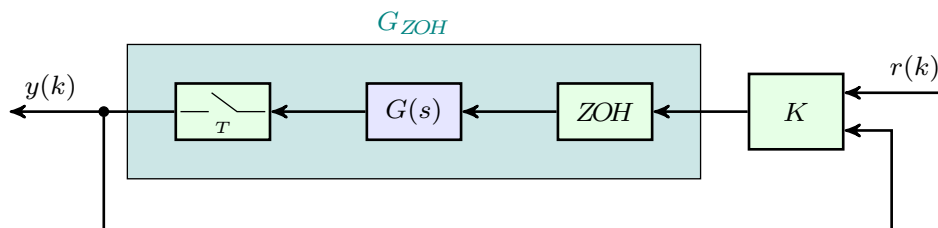


## Digital control system design

Digital controller and continuous plant: closed-loop



Discrete-time equivalence



## Discrete-time state-space models

Plant model:



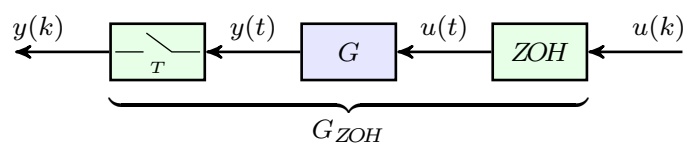
$$x(k+1) = Ax(k) + Bu(k)$$

$$y(k) = Cx(k) + Du(k)$$

The discrete-time state-space system is stable if and only if

$$|\text{eig}(A)| < 1.$$

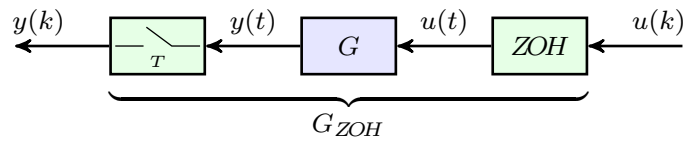
## Zero-order hold equivalence — state space



Integrating  $\Phi(t)$  over a single sample period ( $kT$  to  $kT + T$ ):

$$x(kT + T) = e^{AT} x(kT) + \int_{kT}^{kT+T} e^{A(kT+T-\tau)} Bu(\tau) d\tau,$$

## Zero-order hold equivalence — state space



Integrating  $\Phi(t)$  over a single sample period ( $kT$  to  $kT + T$ ):

$$x(kT + T) = e^{AT} x(kT) + \int_{kT}^{kT+T} e^{A(kT+T-\tau)} B u(\tau) d\tau,$$

$$\left[ \begin{array}{c|c} A & B \\ \hline C & D \end{array} \right] \xrightarrow{\text{ZOH-equivalence}} \left[ \begin{array}{c|c} e^{AT} & \int_0^T e^{A\eta} B d\eta \\ \hline C & D \end{array} \right]$$

MATLAB calculation: `c2d`

## Discrete-time controllers

### Proportional controller

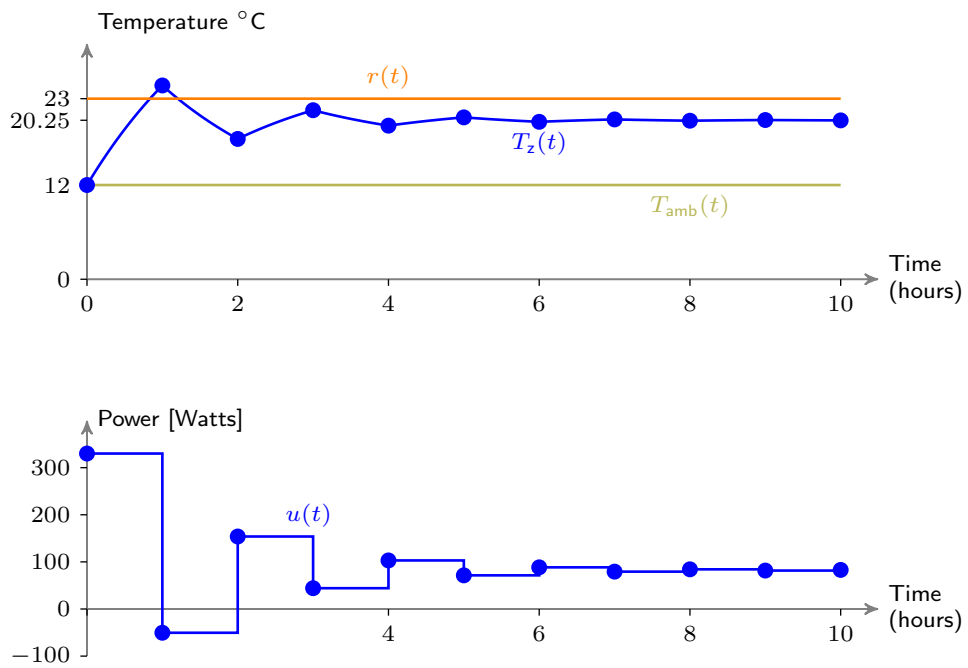
$$u(k) = K_P e(k)$$

### PI controller

$$x_K(k+1) = 1 x_K(k) + T e(k)$$

$$u(k) = K_I x_K(k) + K_P e(k)$$

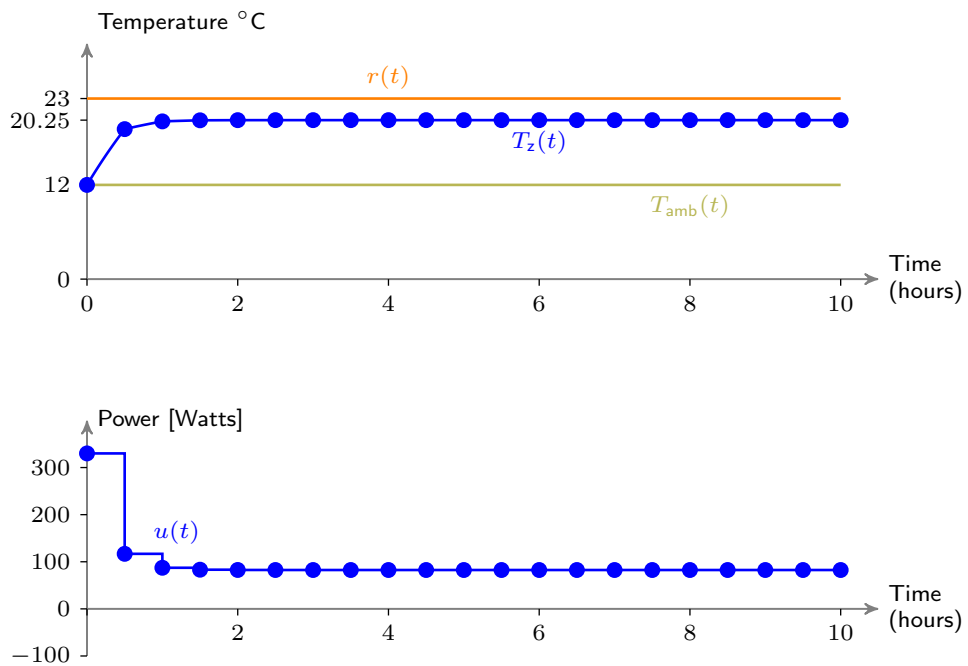
## P-control



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## P-control, faster sampling



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## PI-control, discrete-time

