Control of Low-Inertia Power Systems: Naive & Foundational Approaches

INCITE Seminar @ Universitat Politècnica de Catalunya

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Acknowledgements


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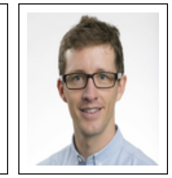
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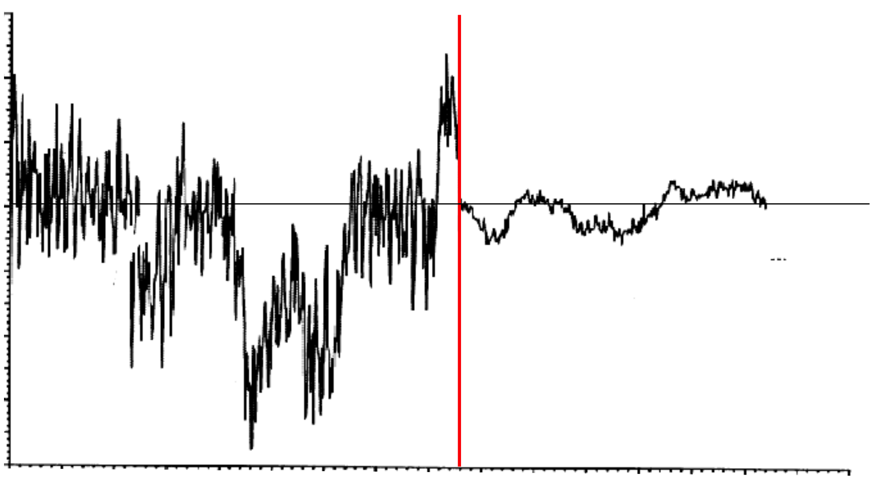
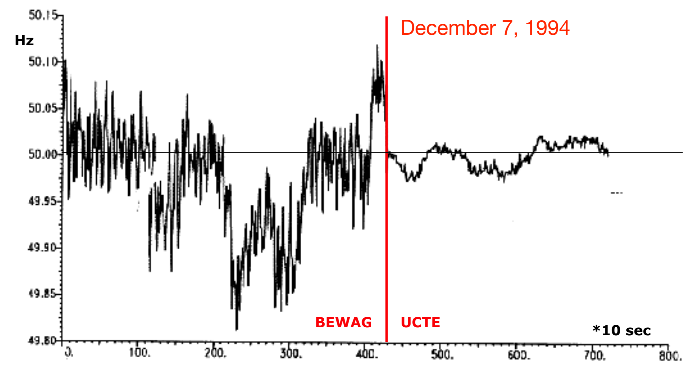
What do we see here?



Frequency of West Berlin when re-connecting to Europe

Source: *Energie-Museum Berlin*



before re-connection: islanded operation based on batteries & single boiler

afterwards connected to European grid based on synchronous generation

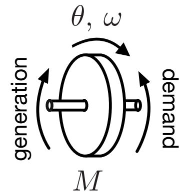
Essentially, the pre/post West Berlin curves date back to. . .

Fact: all of AC power systems built around **synchronous machines**!

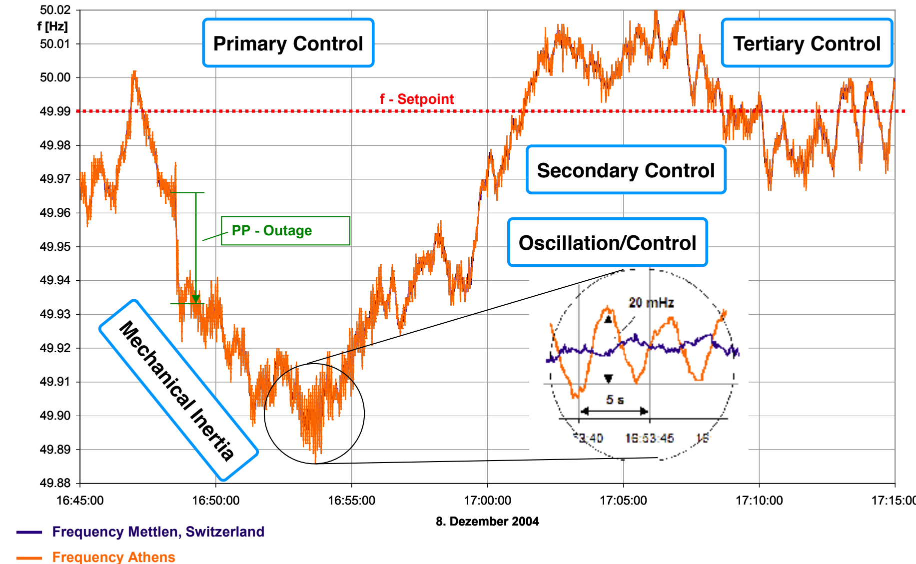
At the heart of it is the generator **swing equation**:

$$M \frac{d}{dt}\omega(t) = P_{\text{generation}}(t) - P_{\text{demand}}(t)$$

change of kinetic energy = instantaneous power balance



Operation centered around bulk synchronous generation



Source: W. Sattinger, Swissgrid

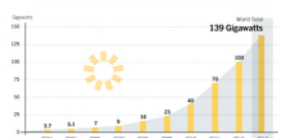
Renewable/distributed/non-rotational generation on the rise

synchronous generator

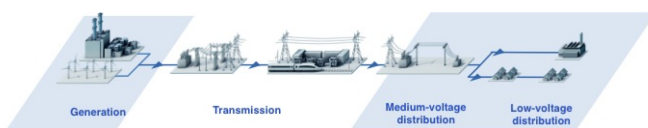
new workhorse

scaling

new primary sources

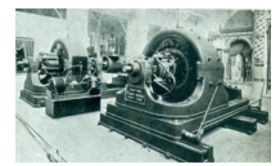


location & distributed implementation



focus today on **non-rotational** generation

The foundation of today's power system



Synchronous machines with rotational **inertia**

$$M \frac{d}{dt}\omega \approx P_{\text{generation}} - P_{\text{demand}}$$

Today's grid operation heavily relies on

1. **robust** stabilization of **frequency** and **voltage** by generator controls
2. **self-synchronization** of machines **through the grid**
3. kinetic energy $\frac{1}{2}M\omega^2$ as **safeguard** against disturbances

We are replacing this solid foundation with . . .

Tomorrow's clean and sustainable power system

Non-synchronous generation connected via **power electronics**

As of today, power electronic converters

1. **lack robust control** for **voltage** and **frequency**
2. **do not** inherently **synchronize** through the grid
3. provide almost **no energy storage**

What could possibly go wrong?

The concerns are not hypothetical: South Australia event

THE AUSTRALIAN
THE HEART OF THE NATION

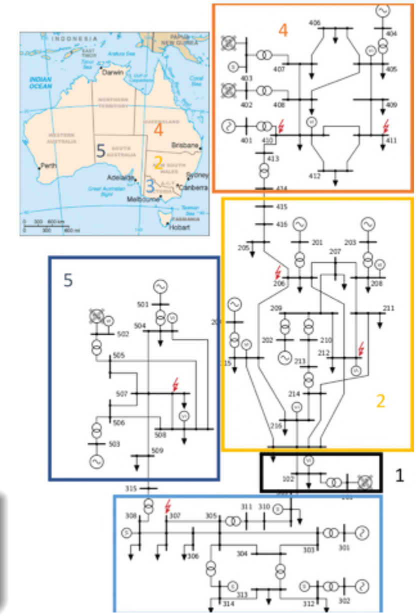
South Australia blackout: renewables don't cope with rapid change report finds

The Australian | 11:44AM December 15, 2016

UPDATE REPORT – BLACK SYSTEM EVENT IN SOUTH AUSTRALIA ON 28 SEPTEMBER 2016

AEMO

AN UPDATE TO THE PRELIMINARY OPERATING INCIDENT REPORT FOR THE NATIONAL ELECTRICITY MARKET. DATA ANALYSIS AS AT 5.00 PM TUESDAY 11 OCTOBER 2016.



my **conclusion** from official report:
blue low-inertia area 5 was not resilient;
conventional system would have survived

Black System Event in South Australia (Sep 2016)

The Sydney Morning Herald

NATIONAL

State in the dark: South Australia's major power outage

theguardian

South Australia

South Australia blackout: entire state left without power after storms

Key events[1]

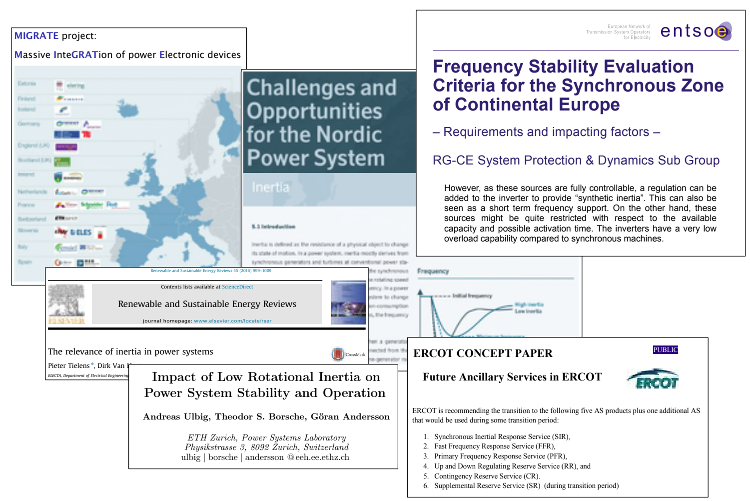
1. intermittent **voltage disturbances** due to line faults
2. loss of **synchronism** between SA and remainder of the grid
3. SA islanded: **frequency collapse** in a **quarter** of a **second**

"**Nine** of the **13** wind farms online **did not ride through** the six **voltage disturbances** experienced during the event."

[1] AEMO: Update Report - Black System Event in South Australia on 28 September 2016

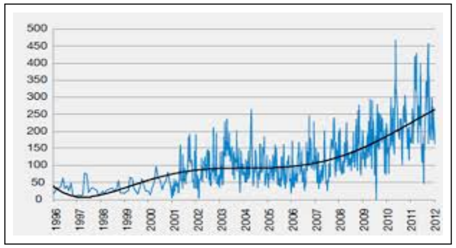
Low inertia issues have been broadly recognized

by TSOs, device manufacturers, academia, funding agencies, etc.

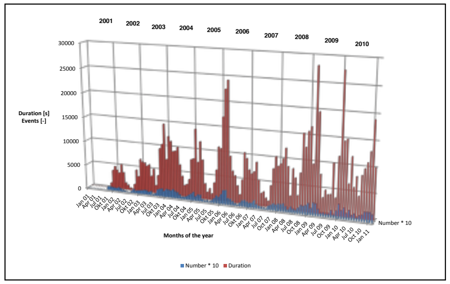


MIGRATE consortium: green-field approach to control of zero-inertia grids

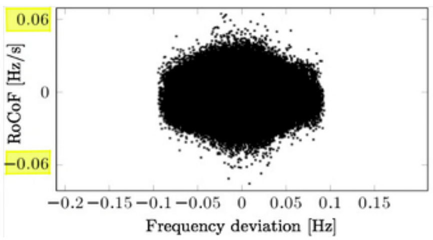
Low-inertia issues close to home



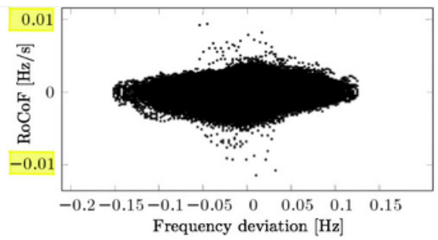
frequency violations in Nordic grid (source: ENTSO-E)



same in Switzerland (source: Swissgrid)



a day in Ireland (source: F. Emiliano)



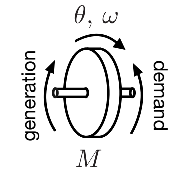
a year in France (source: RTE)

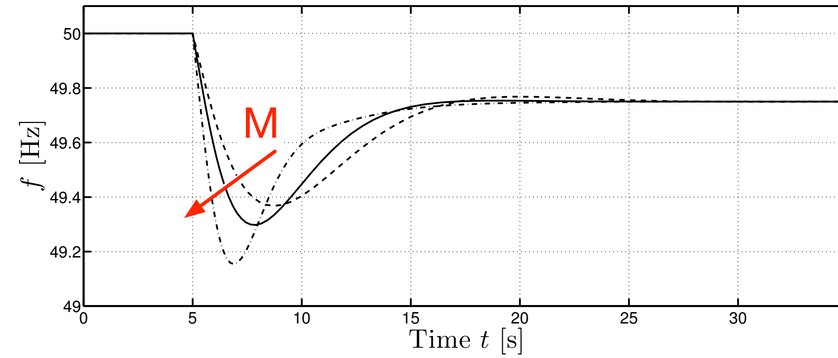
Obvious insight: loss of inertia & frequency stability

We loose our giant electromechanical low-pass filter:

$$\mathbf{M}\,\frac{d}{dt}\,\omega(t) \;=\; P_{\text{generation}}(t) - P_{\text{demand}}(t)$$

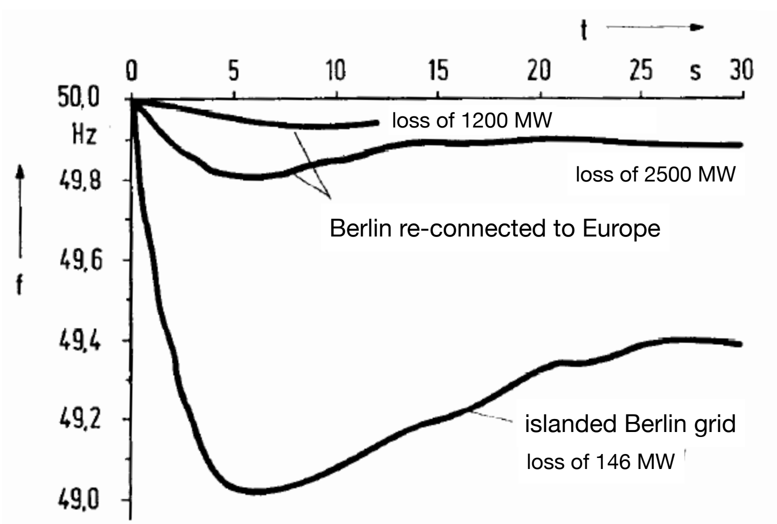
change of kinetic energy = instantaneous power balance





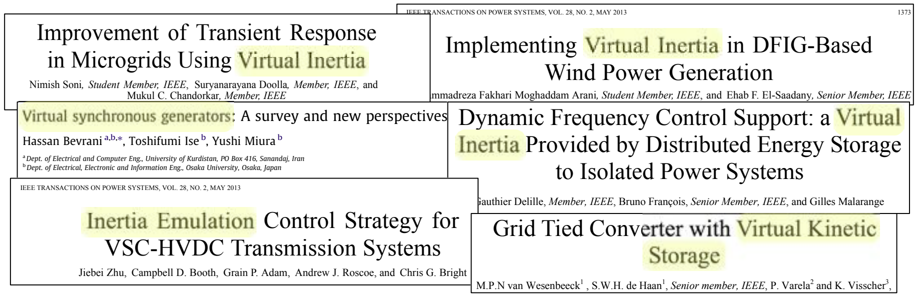
Berlin curves before and after re-connecting to Europe

Source: *Energie-Museum Berlin*



obvious insights lead to obvious (naive) answers

Baseline solution: virtual inertia emulation


IEEE TRANSACTIONS ON POWER SYSTEMS, VOL. 28, NO. 2, MAY 2013

Improvement of Transient Response in Microgrids Using Virtual Inertia

Nimish Soni, Student Member, IEEE, Suryanarayana Doolla, Member, IEEE, and Mukul C. Chandorkar, Member, IEEE

Implementing Virtual Inertia in DFIG-Based Wind Power Generation

...mmadreza Fakhari Moghaddam Arani, Student Member, IEEE, and Ehab F. El-Saadany, Senior Member, IEEE

Virtual synchronous generators: A survey and new perspectives

Hassan Bevrani[a,b,*], Toshifumi Ise[b], Yushi Miura[b]

[a] Dept. of Electrical and Computer Eng., University of Kurdistan, PO Box 416, Sanandaj, Iran
[b] Dept. of Electrical, Electronic and Information Eng., Osaka University, Osaka, Japan

Dynamic Frequency Control Support: a Virtual Inertia Provided by Distributed Energy Storage to Isolated Power Systems

...authier Delille, Member, IEEE, Bruno François, Senior Member, IEEE, and Gilles Malarange

IEEE TRANSACTIONS ON POWER SYSTEMS, VOL. 28, NO. 2, MAY 2013

Inertia Emulation Control Strategy for VSC-HVDC Transmission Systems

Jiebei Zhu, Campbell D. Booth, Grain P. Adam, Andrew J. Roscoe, and Chris G. Bright

Grid Tied Converter with Virtual Kinetic Storage

M.P.N van Wesenbeeck[1], S.W.H. de Haan[1], Senior member, IEEE, P. Varela[2] and K. Visscher[3],

$$M \frac{d}{dt}\omega(t) = P_{\text{generation}}(t) - P_{\text{demand}}(t) \approx \textbf{derivative control} \text{ on } \omega(t)$$

⇒ **focus today: where** to do it? **how** to implement it properly?

. . . we are not just loosing inertia . . . **what else** to do ?

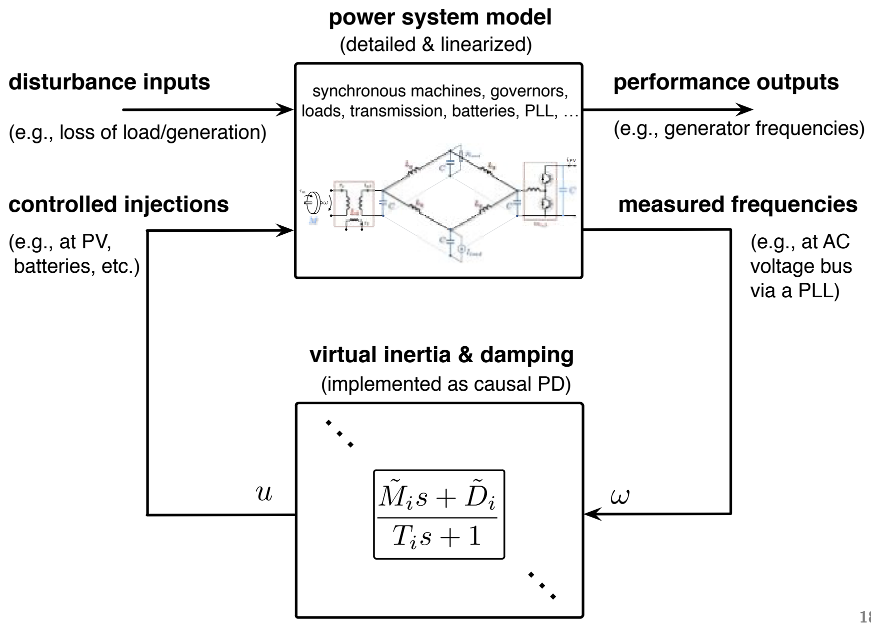
Outline

Virtual inertia is becoming a technology and a product

so let's see how we can make use of it

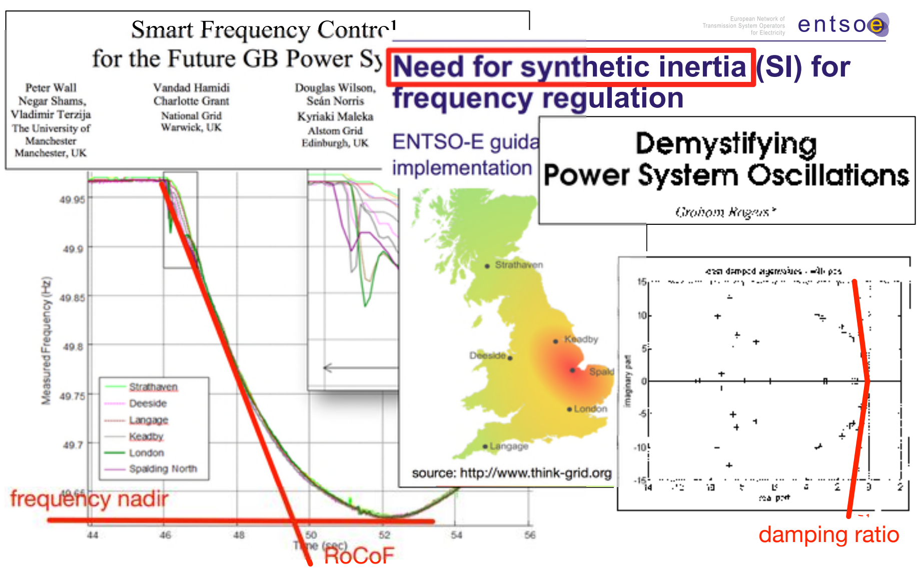
optimal placement of virtual inertia

General power system & inertia emulation model



which metric(s) should our controller optimize ?

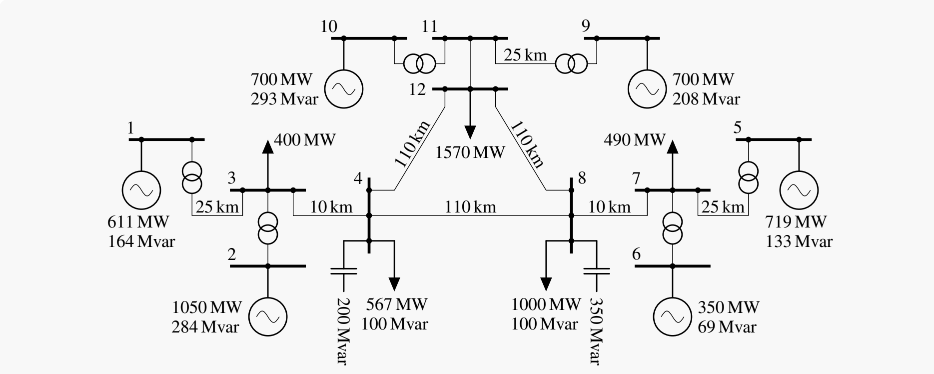
Conventional metrics: spectrum, RoCoF, & total inertia



are these suitable metrics ?

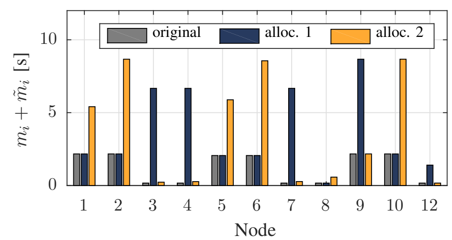
let's look at some simulations

Running example: modified Kundur three-area case study

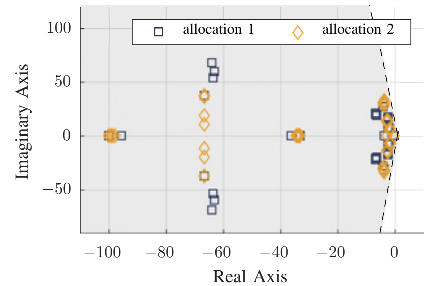


- added third area to standard case
- PLLs at all buses for inertia emulation (overall device response time ∼100ms)
- transformer reactance 0.15 p.u, line impedance (0.0001+0.001i) p.u./km
- original inertia 40s: removed of rotational 28s which can be re-allocated as virtual inertia
- added governors & droop control at all generators

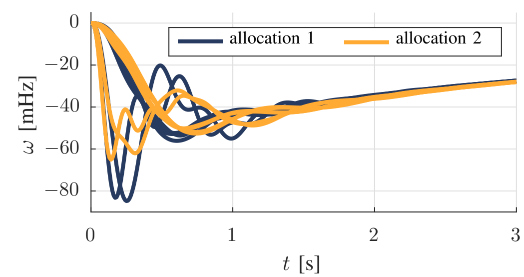
Fact: RoCoF, spectrum, & total inertia are poor metrics



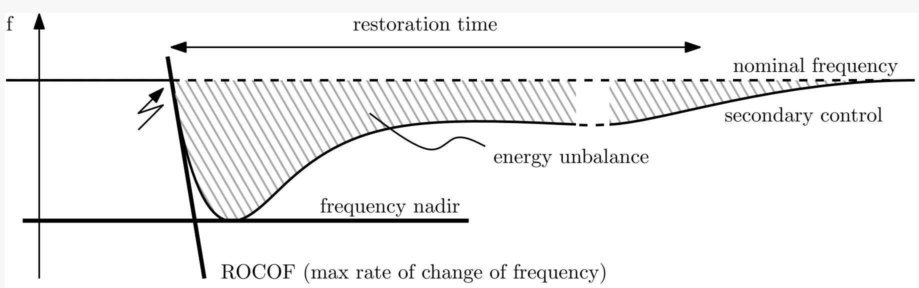
metrics	allocation 1	allocation 2
total inertia	40.85 s	40.85 s
damping ratio	0.1190	0.1206
RoCoF	0.8149 Hz/s	0.8135 Hz/s
ω nadir	-84.8 mHz	-65.1 mHz
peak injection	118.38 MW	7.0446 MW
control effort	15.581	2.699



comparison for 100 MW load step at bus 7



Re-visiting performance metrics for low-inertia systems



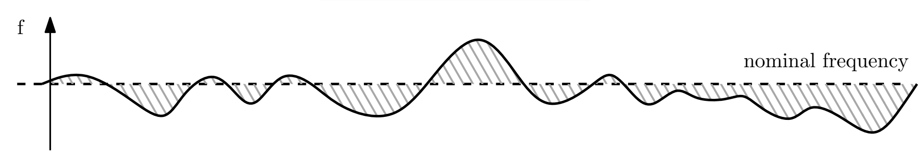
System norm quantifying signal amplifications

disturbances: impulse (fault), step (loss of unit), white noise (renewables) → system → **performance outputs:** integral, peak, ROCOF, restoration time, . . .

Integral-quadratic coherency performance metric

other metrics are poor, hard-to-optimize, & characterize a high (not low) inertia system

$$\int_0^\infty x(t)^T Q\, x(t)\, dt$$

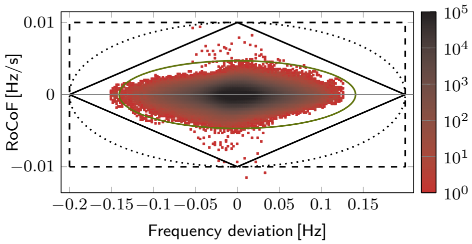


$\mathcal{H}_2$ **system norm** interpretation: η → system → y

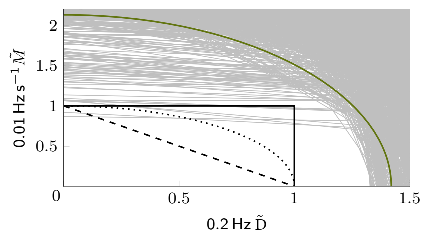
1. **performance output**: $\mathbf{y} = Q^{1/2}x$
2. **impulsive** η (faults) ⟶ output energy $\int_0^\infty \mathbf{y}(t)^\top \mathbf{y}(t)\, dt$
3. **white noise** η (renewables) ⟶ output variance $\lim_{t\to\infty} \mathbb{E}\left(\mathbf{y}(t)^\top \mathbf{y}(t)\right)$

Constraints on control inputs

1. **energy constraint**: $\int_0^\infty u^T R\, u\, dt$ directly captured in $\mathcal{H}_2$ framework
2. **power constraint**: $u_i = \tilde{M}_i\, \dot{\omega}_i + \tilde{D}_i\, \omega_i$ must satisfy $\|u_i(t)\|_{\ell_\infty} \leq \overline{u_i}$



European frequency data (source: RTE)



corresponding bounds on gains

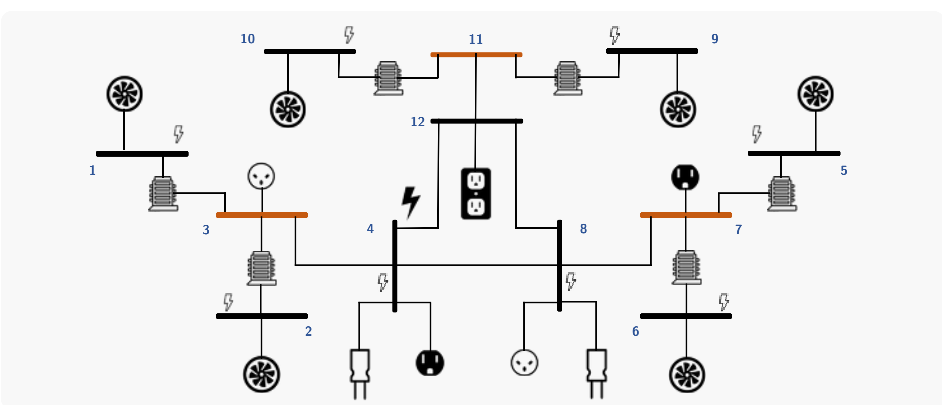
$\Rightarrow$ $\|(\omega_i(t), \dot{\omega}_i(t))\|_1$, $\|(\tilde{D}_i, \tilde{M}_i)\|_\infty$ bounded $\Rightarrow$ $\|u_i(t)\|_{\ell_\infty}$ bounded

3. **budget constraint** for finitely many devices: $\sum_i \overline{u_i} = const.$

(sub)optimize performance and see what we learn

Modified Kundur case study: 3 areas & 12 buses

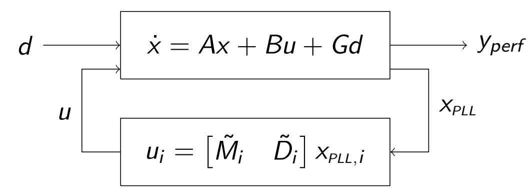
added governors (droop) at generators & PLLs to obtain frequency for inertia emulation



Test case

- **inertia emulation** control via PLL & batteries:

  $$u_i = \begin{bmatrix} \tilde{M}_i & \tilde{D}_i \end{bmatrix} x_{PLL,i}$$

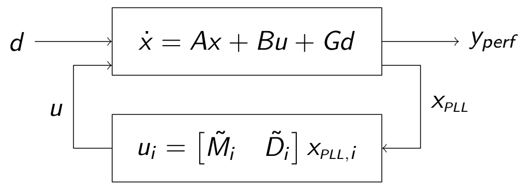


- **dynamics:** swing equation, droop via governor & turbine, and PLL
- **state:** $x = [$ generator states , frequencies , governor control , PLL $]$
- **cost** penalizes frequencies, droop control, & inertia emulation effort:

$$\underbrace{\begin{bmatrix} \omega \\ u_{gov} \\ u \end{bmatrix}}_{y_{perf}} = \underbrace{\begin{bmatrix} 0 & I & 0 & 0 \\ 0 & 0 & K_{gov} & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix}}_{=Q^{1/2}} x + \underbrace{\begin{bmatrix} 0 \\ 0 \\ I \end{bmatrix}}_{=R^{1/2}} u$$

Algorithmic approach to desperate & non-convex problem

- **structured** state-feedback with **constraints** on gains
- **computation** $\mathcal{H}_2$ norm, gradient, & projections:



1. observability and controllability Gramians via **Lyapunov equations**

$$(A - BK)^\top P + P(A - BK) + Q + K^\top RK = 0$$
$$(A - BK)L + L(A - BK)^\top + GG^\top = 0$$

2. $\mathcal{H}_2$ **norm** $J = \text{Trace}(G^\top PG)$ and **gradient** $\nabla_K J = 2(RK - B^\top P)L$

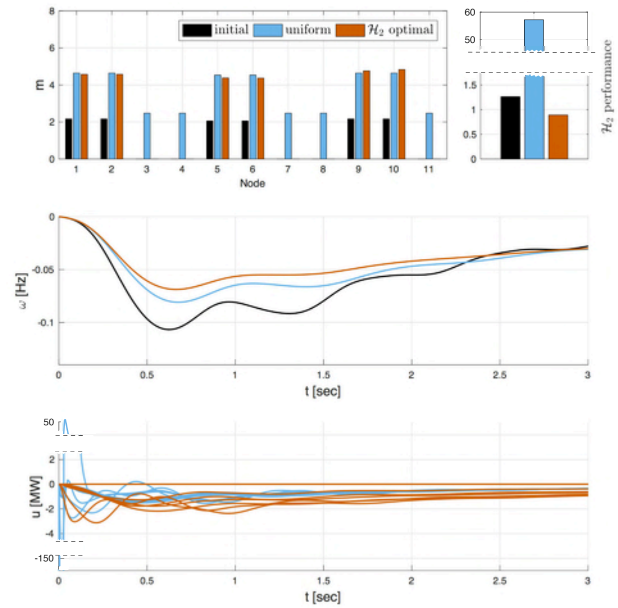
3. **projection** on structural & ∞-norm constraint: $\Pi_{\tilde{M},\tilde{D}}[\nabla_K J]$

$\Rightarrow$ $\tilde{M}$ and $\tilde{D}$ can be optimized by **first-order methods**, IPM, SQP, etc.

Results & insights for the three-area case study

Optimal allocation:
- location of inertia & damping matters
- outperforms heuristic uniform allocation
- need penalty on droop control effort
- power constraint results in $\tilde{D} \approx 2\tilde{M}$

Fault at bus #4:
- strong reduction of frequency deviation
- much less control effort than heuristic



can we make this control design strategy useful ?

Recall: South Australia event

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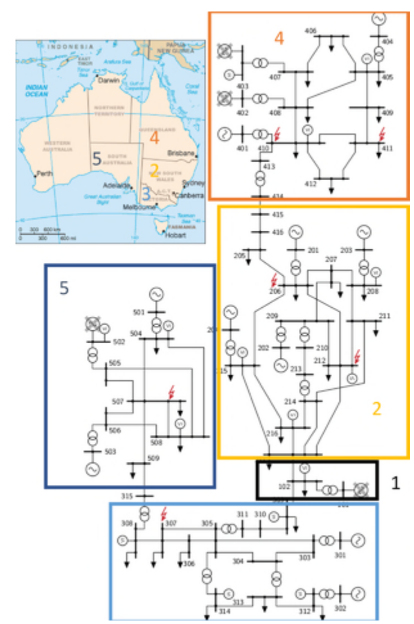
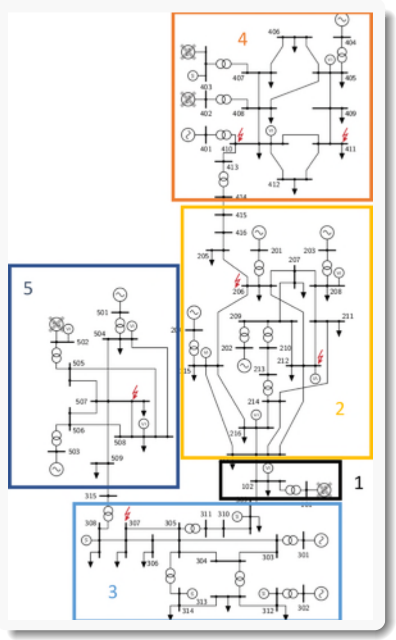


Control & optimization design scale up to large systems

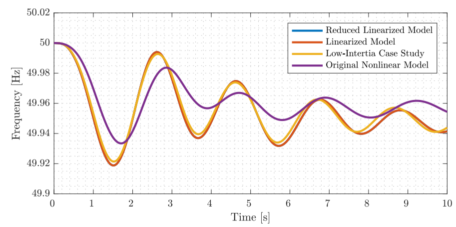


low-inertia **Eastern-Australian grid**:

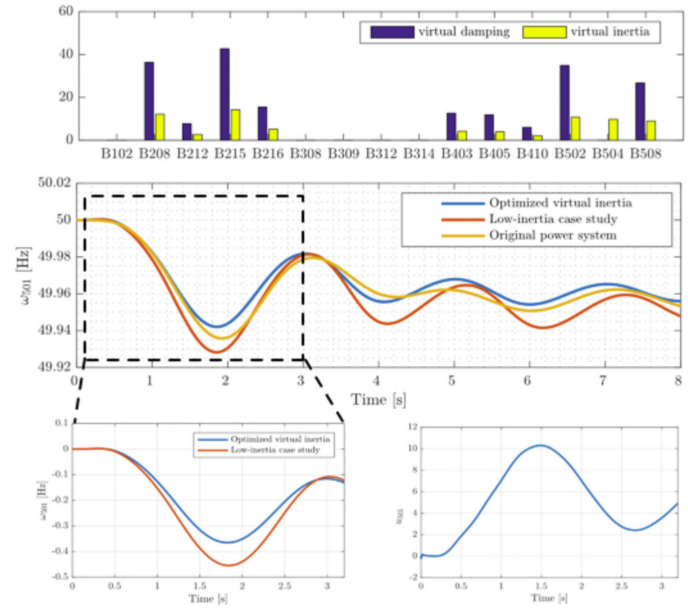
- removed rotational generation at buses 101, 402, 403 and 502
- added controllable power sources with PLLs at 15 buses

tractable model for design:

- linearization of nonlinear model
- balanced reduction to 140 states



$\mathcal{H}_2$-optimal virtual inertia allocation with ℓ_∞ constraints



allocation at core area 2 and critical areas 4 & 5

improves performance of low-inertia & original case

post-fault frequencies & control input well-behaved

placement & metrics matter!

can we get analytic insights ?

Inertia placement in swing equations

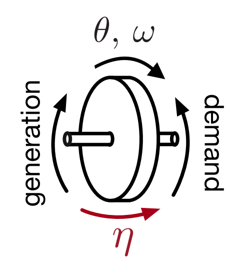
- simplified network swing equation **model**:

$$m_i\ddot{\theta}_i + d_i\dot{\theta}_i = p_{gen,i} - p_{dem,i}$$

generator swing equations

$$p_{dem,i} \approx \sum_j b_{ij}\left(\theta_i - \theta_j\right)$$

linearized DC power flow



- likelihood of **disturbance** at $\#i$: $\eta_i \geq 0$ (available from TSO data)
- $\mathcal{H}_2$ performance **metric**: $\int_0^\infty \sum_{i,j} a_{ij}(\theta_i - \theta_j)^2 + \sum_i s_i\dot{\theta}_i^2\, dt$
- **decision variable** is inertia: $m_i \in [\underline{m_i}\,,\,\overline{m_i}]$

  (additional nonlinearity: enters as m_i^{-1} in constraints & objective)

Closed-form results for cost of primary control

recall: primary control $d_i \dot{\theta}_i$ **effort** was crucial

$$\int_0^\infty \dot{\theta}(t)^\top D\,\dot{\theta}(t)\,dt$$

(computations show that insights *roughly* generalize to other costs)

allocation: the primary control effort $\mathcal{H}_2$ optimization reads equivalently as

$$\begin{aligned} \underset{m_i}{\text{minimize}} \quad & \textstyle\sum_i \frac{\eta_i}{m_i} \\ \text{subject to} \quad & \textstyle\sum_i m_i \le m_{\text{bdg}} \\ & \underline{m_i} \le m_i \le \overline{m_i} \end{aligned}$$

key take-away is **disturbance matching**:

- optimal allocation $m_i^\star \propto \sqrt{\eta_i}$ or $m_i^\star = \min\{m_{\text{bdg}}, \overline{m_i}\}$

$\Rightarrow$ disturbance profile known from historic data, but rare events are crucial

- suggests **robust** $\min_m \max_\eta$ **allocation** to prepare for worst case

$\Rightarrow$ valley-filling solution: $\eta_i^\star / m_i^\star = const.$ (up to constraints)

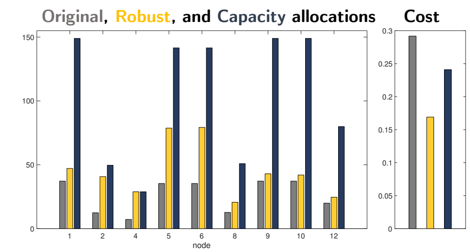
Robust min - max allocation for three-area case study

Scenario: fault (impulse) can occur at any single node

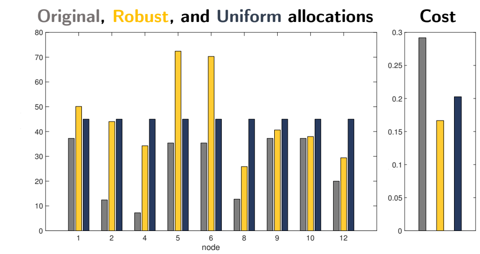
- disturbance set
  $\eta \in \{e_1 \cup \cdots \cup e_{12}\}$

$\Rightarrow$ **min/max** over convex hull

- inertia **capacity constraints**
- robust inertia allocation **outperforms heuristic** max-capacity allocation
- results become **intuitive**: valley-filling property
- same for uniform allocation



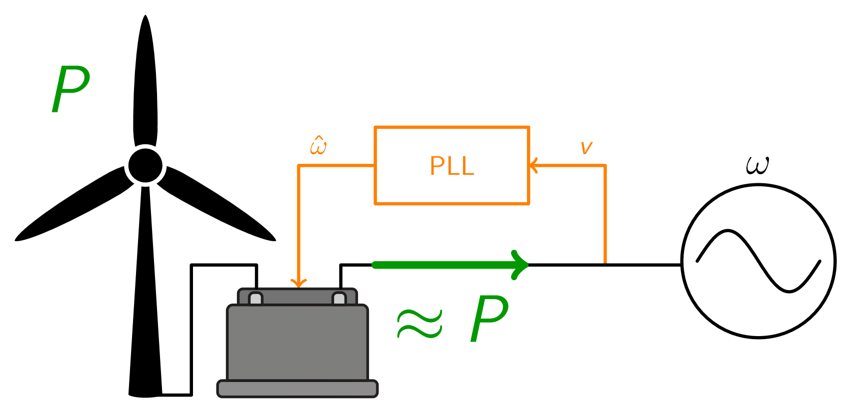
allocation subject to capacity constraints



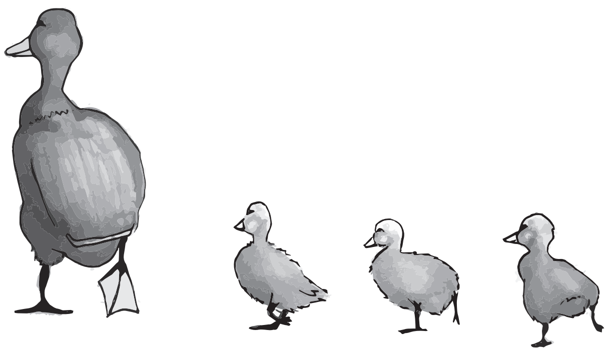
allocation subject to the budget constraint

Outline

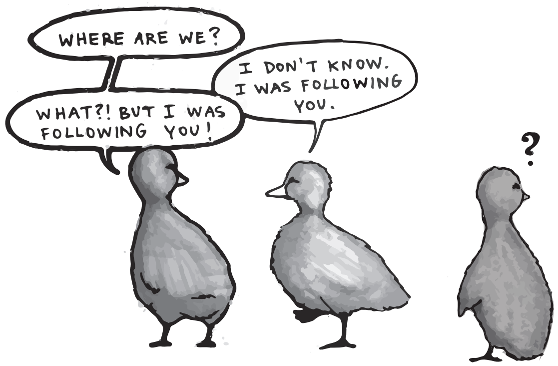
Grid-following inverters



A stiff grid with grid-following sources . . .



If everyone follows...



we are not just loosing inertia

——————————————

interestingly, many so-called “virtual inertia” controllers are grid-following

design of robust grid-forming mechanisms

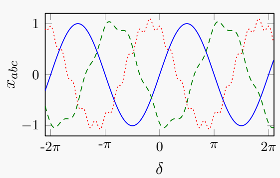
Modeling: signal space in three-phase AC power systems

three-phase AC

$$\begin{bmatrix} x_a(t) \\ x_b(t) \\ x_c(t) \end{bmatrix} = \begin{bmatrix} x_a(t+T) \\ x_b(t+T) \\ x_c(t+T) \end{bmatrix}$$

periodic with 0 average

$$\frac{1}{T}\int_0^T x_i(t)dt = 0$$

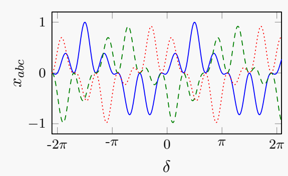


balanced (nearly true)

$$= A(t) \begin{bmatrix} \sin(\delta(t)) \\ \sin(\delta(t) - \frac{2\pi}{3}) \\ \sin(\delta(t) + \frac{2\pi}{3}) \end{bmatrix}$$

so that

$$x_a(t)+x_b(t)+x_c(t)=0$$

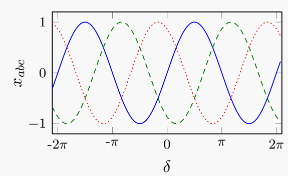


synchronous (desired)

$$= A \begin{bmatrix} \sin(\delta_0 + \omega_0 t) \\ \sin(\delta_0 + \omega_0 t - \frac{2\pi}{3}) \\ \sin(\delta_0 + \omega_0 t + \frac{2\pi}{3}) \end{bmatrix}$$

const. freq & amp

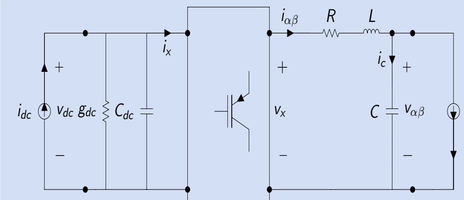
$\Rightarrow$ const. in rot. frame



assumption: signals are balanced $\Rightarrow$ 2d-coordinates $x(t) = [x_\alpha(t)\ x_\beta(t)]$

(equivalent representation: complex-valued polar/phasor coordinates)

Averaged power converter model



DC cap & AC filter equations:

$$C_{dc}\dot{v}_{dc} = -G_{dc}v_{dc} + i_{dc} - \frac{1}{2}m^\top i_{\alpha\beta}$$

$$L\dot{i}_{\alpha\beta} = -Ri_{\alpha\beta} + \frac{1}{2}mv_{dc} - v_{\alpha\beta}$$

$$C\dot{v}_{\alpha\beta} = -i_{load} + i_{\alpha\beta}$$

modulation: $v_x = \frac{1}{2}mv_{dc}$, $i_x = \frac{1}{2}m^\top i_{\alpha\beta}$

control/dist. inputs: (i_{dc}, i_{load})

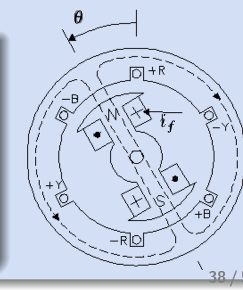
synchronous generator:
mechanical
+ stator flux
+ AC cap

$$\dot{\theta} = \omega$$

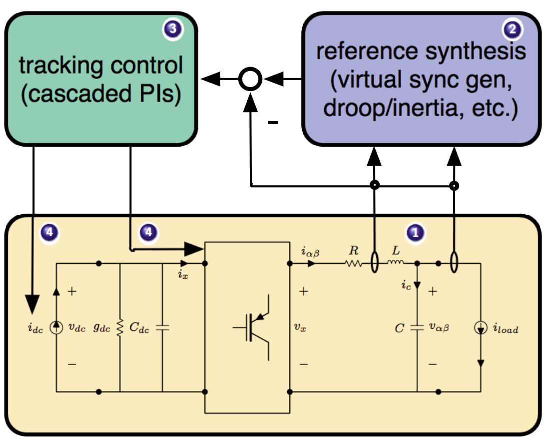
$$M\dot{\omega} = -D\omega + \tau_m + i_{\alpha\beta}^\top L_m i_f \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$

$$L_s\dot{i}_{\alpha\beta} = -Ri_{\alpha\beta} - v_{\alpha\beta} - \omega L_m i_f \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$

$$C\dot{v}_{\alpha\beta} = -i_{load} + i_{\alpha\beta}$$



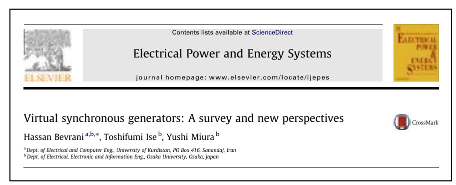
Standard power electronics control would continue by



1. acquiring & processing of **AC measurements**
2. synthesis of **references** (voltage/current/power)
3. **track** error signals at converter terminals
4. **actuation** via modulation (inner loop) and/or via DC source (outer loop)

I guess you can see the **problems building up** ...

Challenges in power converter implementations



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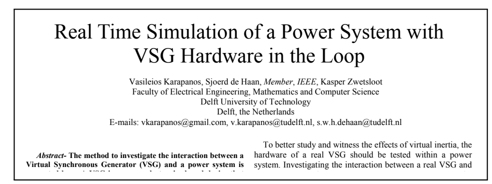
Virtual synchronous generators: A survey and new perspectives

Hassan Bevrani, Toshifumi Ise, Yushi Miura



Real Time Simulation of a Power System with VSG Hardware in the Loop

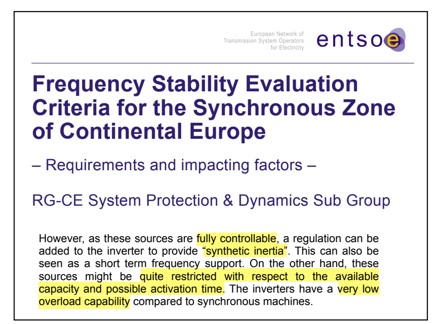
Vasileios Karapanos, Sjoerd de Haan, *Member, IEEE*, Kasper Zwetsloot

Faculty of Electrical Engineering, Mathematics and Computer Science

Delft University of Technology

Delft, the Netherlands

1. **delays** in measurement acquisition, signal processing, & actuation
2. **accuracy** in AC measurements (averaging over multiple cycles)
3. **constraints** on currents, voltages, power, etc.
4. **certificates** on stability, robustness, & performance



entsoe

Frequency Stability Evaluation Criteria for the Synchronous Zone of Continental Europe

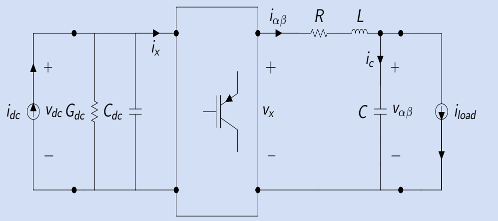
– Requirements and impacting factors –

RG-CE System Protection & Dynamics Sub Group

However, as these sources are fully controllable, a regulation can be added to the inverter to provide "synthetic inertia". This can also be seen as a short term frequency support. On the other hand, these sources might be quite restricted with respect to the available capacity and possible activation time. The inverters have a very low overload capability compared to synchronous machines.

let's do **something smarter** ...

See the similarities & the differences ?



DC cap & AC filter equations:

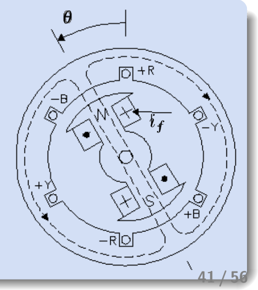
$$C_{dc}\dot{v}_{dc} = -G_{dc}v_{dc} + i_{dc} - \frac{1}{2}m^\top i_{\alpha\beta}$$
$$L\dot{i}_{\alpha\beta} = -Ri_{\alpha\beta} + \frac{1}{2}mv_{dc} - v_{\alpha\beta}$$
$$C\dot{v}_{\alpha\beta} = -i_{load} + i_{\alpha\beta}$$

modulation: $v_x = \frac{1}{2}mv_{dc}$, $i_x = \frac{1}{2}m^\top i_{\alpha\beta}$

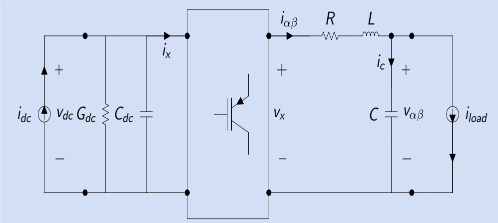
passive: $(i_{dc}, i_{load}) \to (v_{dc}, v_{\alpha\beta})$

synchronous generator: mechanical + stator flux + AC cap

$$\dot{\theta} = \omega$$
$$M\dot{\omega} = -D\omega + \tau_m + i_{\alpha\beta}^\top L_m i_f \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$
$$L_s\dot{i}_{\alpha\beta} = -Ri_{\alpha\beta} - v_{\alpha\beta} - \omega L_m i_f \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$
$$C\dot{v}_{\alpha\beta} = -i_{load} + i_{\alpha\beta}$$



Model matching (≠ emulation) as inner control loop



DC cap & AC filter equations:

$$C_{dc}\dot{v}_{dc} = -G_{dc}v_{dc} + i_{dc} - \frac{1}{2}m^\top i_{\alpha\beta}$$
$$L\dot{i}_{\alpha\beta} = -Ri_{\alpha\beta} + \frac{1}{2}mv_{dc} - v_{\alpha\beta}$$
$$C\dot{v}_{\alpha\beta} = -i_{load} + i_{\alpha\beta}$$

matching control: $\dot{\theta} = K_m \cdot v_{dc}$, $m = \hat{m} \cdot \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$ with $K_m, \hat{m} > 0$

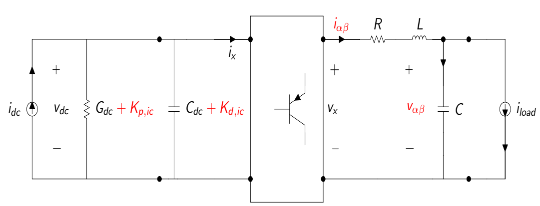
⇒ **equivalent** inertia $M = \frac{C_{dc}}{K_m^2}$, imbalance signal $\omega = K_m \cdot v_{dc}$, etc.

⇒ **pros:** uses physical storage, uses DC measurements, & remains passive

Further properties of machine matching control

❶ base for **outer loops**

⇒ $i_{dc} = \textbf{PD}(v_{dc})$ gives virtual inertia & damping

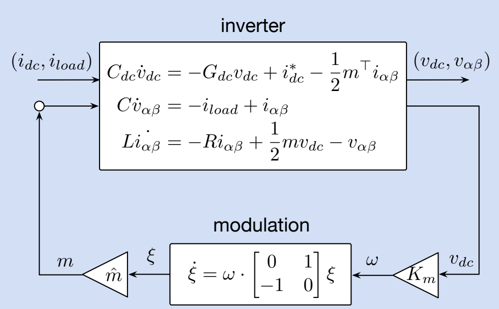


❷ reformulation of

$$m = \hat{m} \cdot \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$

as adaptive **oscillator**:

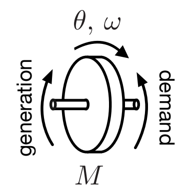
$$\dot{m} = K_m\, v_{dc} \cdot \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} m$$



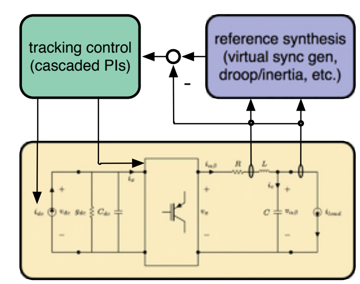
Summary: bottlenecks to inertia emulation

power system model on **grid level:**

$$M\frac{d}{dt}\omega = P_{\text{generation}} - P_{\text{demand}}$$



inertia emulation on **device level:**



- **I/O mismatch:** none of the converter inputs or outputs are present in the swing-equation, e.g., frequency is not a state in the converter
- **inertia emulation** à la PD problematic both in theory & practice

⇒ maybe **matching control** $\dot{m} = K_m\, v_{dc} \cdot \begin{bmatrix} 0 & 1 \\ -1 & 0 \end{bmatrix} m$ was quite clever ?

Outline

Introduction

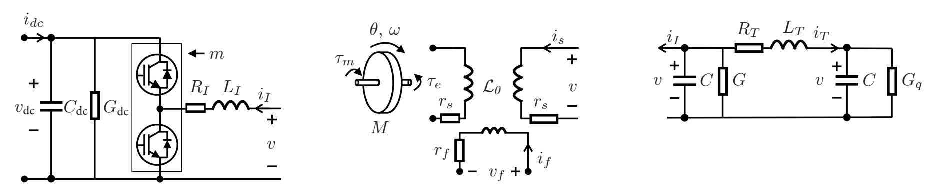
System Level: Optimal Placement of Virtual Inertia
network, disturbances, & performance metrics matter

Device Level: Proper Virtual Inertia Emulation Strategy
maybe we should not think about frequency and inertia

A Foundational Control Approach
restart from scratch for low-inertia systems

Conclusions

Low-inertia power system model from first principles



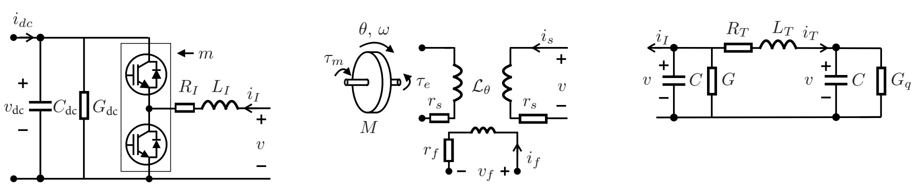
- balanced three-phase system
  - (α, β) coordinates
- synchronous machines
  - first principle, 5th order
- DC/AC inverters
  - averaged-switched
- nonlinear loads $G(\|v\|)$
- voltage bus charge dynamics
- dynamic transmission lines: Π-model

Port-Hamiltonian model

$$\dot{x} = \Big(J(x,u) - R(x)\Big)\,\nabla H(x) + g(x)u$$

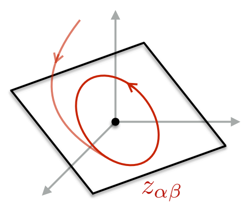
nonlinear & large, but insightful

Desired steady-state locus & control specifications



steady-state specifications for nonlinear system:

- synchronous frequency
- constant amplitude
- three-phase balanced



AC quantities v, i_s, i_I, i_T:

$$\dot{z}_{\alpha\beta} = \omega_0 \cdot \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} z_{\alpha\beta}$$

rotor angles: $\dot{\theta} = \omega_0$

DC quantities v_{dc}, v_f, ω: $\dot{z} = 0$

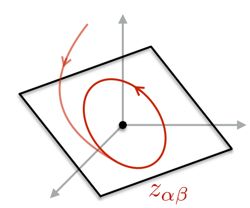
desired dynamics: $\dot{x} = f_{\text{des}}(x, \omega_0)$

controls i_{dc}, m, τ_m, i_f to be found

Proving the obvious (?)

- **steady-state locus**: physics & desired closed-loop vector field coincide (point-wise in time) on set

$$\mathcal{S} := \big\{(x, u, \omega_0) : \; f_{\text{phys}}(x, u) = f_{\text{des}}(x, \omega_0)\big\}$$



- **control-invariance**: steady-state operation $(x, u, \omega_0) \in \mathcal{S}$ for all time **if and only if**

  1. **synchronous frequency** ω_0 is constant
  2. **network** satisfies power flow equations with impedances $R + \omega_0 JL$
  3. at each **generator**: constant torque τ_m & excitation i_f
  4. at each **inverter**: constant DC current i_{dc} & inverter duty cycle with

  constant amplitude & synchronous frequency: $\dot{m} = \omega_0 \cdot \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix} m$

  ⇒ **internal models** & feedforward **input-to-steady-state map**

Reduction to a tractable model for synthesis

- **internal oscillator model** for inverter duty cycle with inputs ω_m, $\hat{m}$

$$\dot{\theta}_I = \omega_m, \quad m = \hat{m} \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$

- **model reduction** steps

  1. **rotating coordinate frame** with synchronous frequency ω_0

     $\Rightarrow$ time scales of AC quantities scaled by $1/\omega_0$
  2. **DC/AC time-scale separation** via singular perturbation ($\epsilon \to 0$)

     slow DC variables: $x_r = (\theta, \omega, i_f, \theta_I, v_{dc})$, $\quad \dot{x}_r = f_z(x_r, z_{\alpha,\beta}, u)$

     fast AC variables: $z_{\alpha,\beta} = (i_s, i_I, v, i_T)$, $\quad \epsilon\, \dot{z}_{\alpha,\beta} = f_{\alpha,\beta}(x_r, z_{\alpha,\beta}, u)$
  3. reformulation via **relative angles** δ with respect to synchronous motion

Insights from reduced model: $v_{dc} \propto$ power imbalance

- **nonlinear reduced order model** in rotating frame:

$$\begin{aligned} \dot{\theta} &= \omega \\ M\dot{\omega} &= -D\omega + \tau_m - \tau_e(x_r, u) \\ L_f \dot{i}_f &= -R_f i_f + v_f - v_{EMF}(x_r, u) \\ \dot{\theta}_I &= \omega_m \\ C_{dc}\dot{v}_{dc} &= -G_{dc} v_{dc} + i_{dc} - i_{sw}(x_r, u) \end{aligned}$$

- **interconnection** via τ_e, i_{sw}, v_{EMF}
- **analogies**: suggest matching control: $\omega_m \sim v_{dc}$

generator	inverter	interpretation
$\frac{1}{2}M\omega^2$	$\frac{1}{2}C_{dc}v_{dc}^2$	energy stored in device
τ_m	i_{dc}	energy supply
τ_e	i_{sw}	energy flow to grid
ω	v_{dc}	power imbalance

Completing the control design

Thus far:

1. desired **steady-state locus** requires internal oscillator model

$$\dot{\theta}_I = \omega_m, \quad m = \hat{m} \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$$

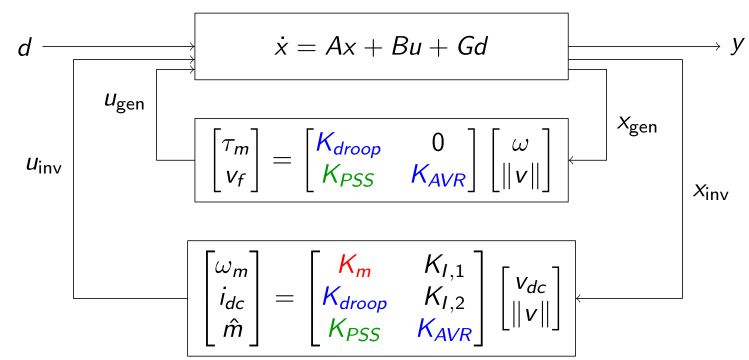
2. **converter/generator analogies** suggest model matching control

$$\omega_m = K_m \cdot (v_{dc} - v_{dc}^*)$$

Remaining steps:

3. **performance** requires design of structured & optimal MIMO control

Decentralized MIMO control architecture

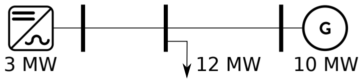


- **states** $x = (\delta, \omega, i_f, v_{dc}, \|v\|)$ & **output** $y = (\omega, v_{dc}, \|v\|)$
- included measurement devices for **AC voltage magnitude** $\|v\|$
- **$\mathcal{H}_2$-optimal tuning** of decentralized MIMO converter controller

Illustrative conceptual example

test case:

- generator & inverter
- impedance load
- 10% load increase at $t=0$

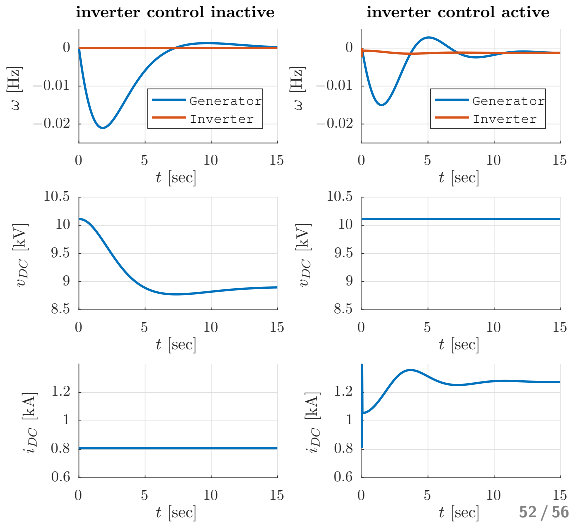


no inverter control:

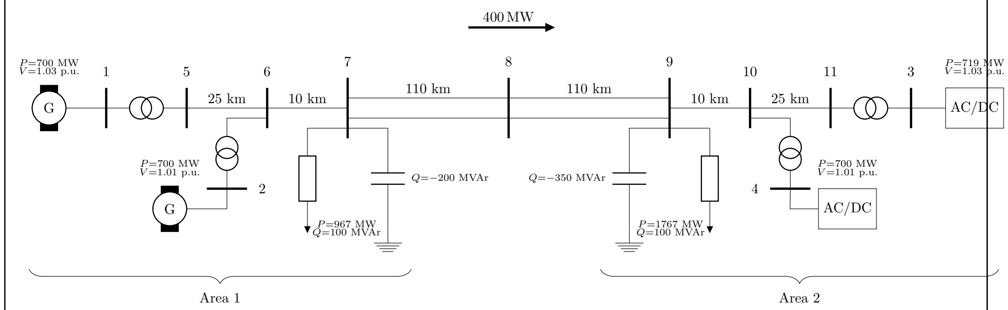
- ω_m and i_{dc} constant
- power imbalance: ω_G, v_{dc}
- governor stabilizes ω_G

controlled inverter:

- reduced peak in ω_G
- v_{dc} stabilized via i_{dc}
- ω_m and ω_G synchronize

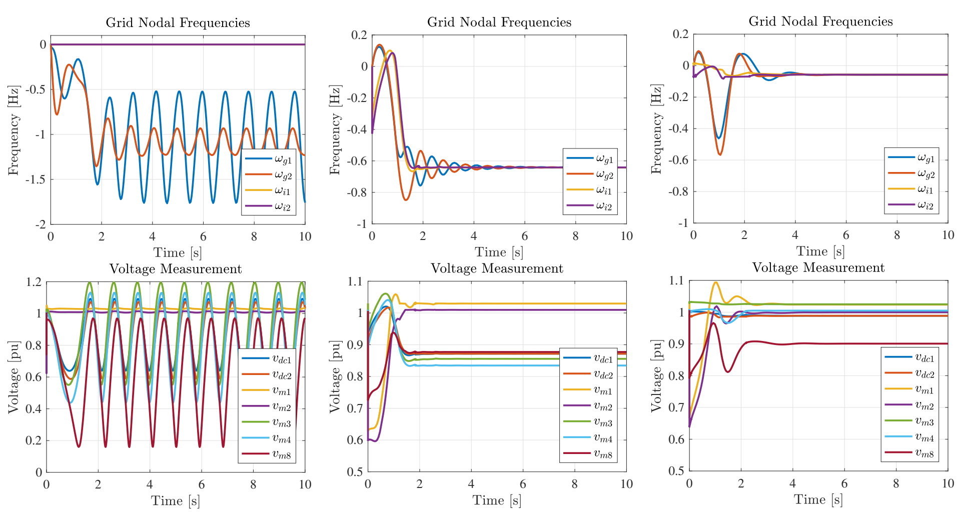


Modified Kundur two-area case study



- standard line parameters and power flows
- synchronous machines with **droop control** and **voltage regulator**
- two **synchronous machines replaced by DC/AC inverters**
- all **dirt effects** modeled: saturation, nonlinearities, etc.
- simulation scenarios: **load step** ($\times 2$) & **outage** of synchronous machine

Scenario: load step & different converter controllers

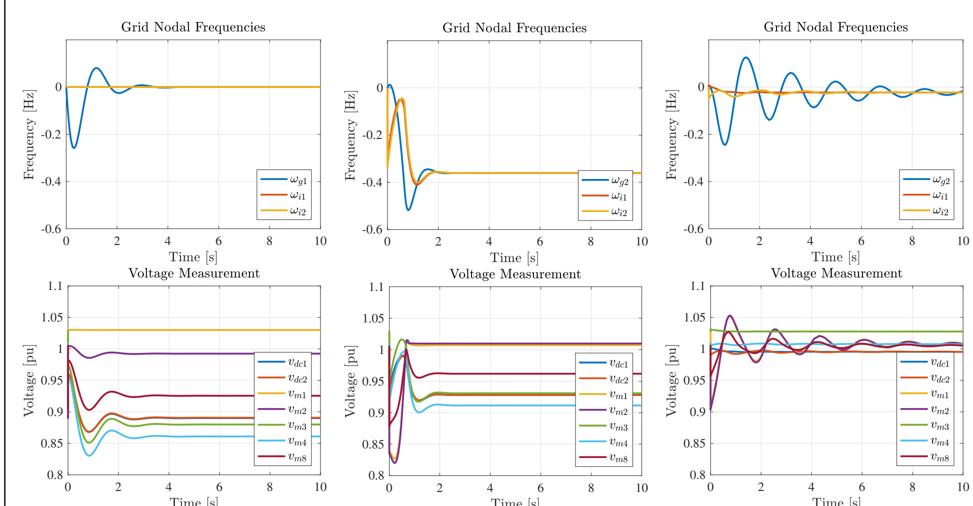


feedforward control (power point tracking)

matching control & un-tuned MIMO gains

$\mathcal{H}_2$-optimal control (all gains tuned)

Scenario: outage of a synchronous machine



feedforward control (power point tracking)

matching control & un-tuned MIMO gains

$\mathcal{H}_2$-optimal control (all gains tuned)

conclusions

Conclusions on virtual inertia emulation

Where to do it?

1. $\mathcal{H}_2$-optimal (non-convex) allocation
2. numerical approach via gradient computation
3. closed-form results for cost of primary control

How to do it?

1. down-sides of naive inertia emulation
2. machine matching reveals power imbalance in DC voltage

What else to do?

1. first-principle low-inertia system model
2. nonlinear steady-state control specifications
3. reduction to tractable model for synthesis
4. first promising controller synthesis:
   internal model + matching + $\mathcal{H}_2$ performance loops