Automatic Control Laboratory ETH Zurich Prof. J. Lygeros D-ITET Winter 2018/2019 7.02.2019

Exercise

25 Points

Signals and Systems II

This sheet is provided to you for ease of reference only. *Do not* write your solutions here.

Exercise 1

Consider t	the d	liscrete	time	linear	system
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$$\begin{cases} x_{k+1} = Ax_k + Bu_k \\ y_k = Cx_k + Du_k \end{cases}$$
(1)

1 | 2 | 3

8 9 8

where $x_k \in \mathbb{R}^n$, $u_k \in \mathbb{R}^m$, $y_k \in \mathbb{R}^p$, $A \in \mathbb{R}^{n \times n}$, $B \in \mathbb{R}^{n \times m}$, $C \in \mathbb{R}^{p \times n}$, and $D \in \mathbb{R}^{p \times m}$.

1. A discrete time observer constructs an estimate \hat{x}_k of the state x_k of the form

$$\begin{cases} \hat{x}_{k+1} = A\hat{x}_k + Bu_k + L(y_k - \hat{y}_k) \\ \hat{y}_k = C\hat{x}_k + Du_k \end{cases}$$

starting with $\hat{x}_0 = 0$. Derive the dynamics of the error $e_k = x_k - \hat{x}_k$. Under what conditions will \hat{x}_k converge to x_k as k tends to infinity?

2. Consider now the system (1) with

$$A = \begin{bmatrix} 0 & 0 & -9 \\ 1 & 0 & -15 \\ 0 & 1 & -7 \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix}$$
(2)

$$C = \begin{bmatrix} 0 & 0 & 1 \end{bmatrix} \qquad D = 0$$

Is the system observable? Is it controllable? Show that the open-loop system has poles at -1 + j0, -3 + j0, and -3 + j0. What does this mean for the stability of the system?

3. Design an observer of the form given in part 1 for the system in part 2. What dimensions should the matrix L have? Select the entries of the matrix L so that the error dynamics have all eigenvalues equal to 0.5.

Exercise 2

1	2	3	4	5	Exercise
5	4	4	8	4	25 Points

Figure 1 shows a water storage system consisting of a cylindrical tank which has constant surface area A_t . Water flows into the tank at a fixed mass-flow rate q_{in} . The mass-flow rate at which the water flows out of the tank can be controlled with a valve whose outflow is given by

$$q_{\rm out}(t) = \rho A_v \sqrt{2gh(t)} v(t),$$

where h(t) is the height of water in the tank and

- ρ water density,
- A_v cross section area of the fully open valve,
- g acceleration due to gravity

are constants. The valve position $v(t) \in [0, 1]$ can be controlled with a servo motor with the transfer function

$$G(s) = rac{V(s)}{U(s)} = rac{2}{s+30}$$

where u(t) is the input voltage to the motor.



Figure 1: Water storage system.

1. Show that the system dynamics takes the form

$$\dot{h}(t) = f_1(h(t), v(t), u(t)) = \frac{q_{\text{in}}}{\rho A_t} - \frac{A_v}{A_t} \sqrt{2gh(t)} v(t),$$

$$\dot{v}(t) = f_2(h(t), v(t), u(t)) = -30v(t) + 2u(t).$$

- 2. Explain whether the system above is
 - (a) linear or nonlinear,
 - (b) time-variant or time-invariant.
- 3. Compute the valve position \bar{v} that maintains the water-level at a constant height \bar{h} . What is the input voltage \bar{u} in that case?

4. Linearize the system around the steady state computed in part 3, *i.e.* compute the matrices A and B in

$$\frac{\mathrm{d}}{\mathrm{d}t} \left(\begin{bmatrix} \delta h(t) \\ \delta v(t) \end{bmatrix} \right) = \underbrace{\begin{bmatrix} \frac{\partial f_1(h,v,u)}{\partial h} & \frac{\partial f_1(h,v,u)}{\partial v} \\ \frac{\partial f_2(h,v,u)}{\partial h} & \frac{\partial f_2(h,v,u)}{\partial v} \end{bmatrix}}_{A} \begin{vmatrix} h = \bar{h} \\ \frac{h = \bar{h}}{\delta v(t)} \end{bmatrix} + \underbrace{\begin{bmatrix} \frac{\partial f_1(h,v,u)}{\partial u} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix}}_{B} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix}_{A} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix}_{B} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix}_{A} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{bmatrix} \begin{vmatrix} h = \bar{h} \\ \frac{\partial f_2(h,v,u)}{\partial u} \end{vmatrix}$$

where $\delta h(t) \coloneqq h(t) - \bar{h}$, $\delta v(t) \coloneqq v(t) - \bar{v}$, and $\delta u(t) \coloneqq u(t) - \bar{u}$.

5. Is the linearized system stable? What can you infer about the stability of the non-linear system?

Exercise 3

1	2	3	4	5	Exercise
3	3	7	8	4	25 Points

Consider the following nonlinear differential equation:

$$\ddot{y}(t) + c\dot{y}(t) + \sin(y(t)) = 0,$$
(3)

where $y(t) \in \mathbb{R}$ for $t \ge 0$, and $c \in \mathbb{R}$.

1. By defining states $x_1(t) = y(t)$ and $x_2(t) = \dot{y}(t)$, write equation (3) in the form

$$\dot{x}(t) = f(x(t)),$$

where $x(t) = (x_1(t), x_2(t))$.

- 2. Find all equilibrium points for the system above.
- 3. Determine the stability of the equilibrium point x = (0, 0) for c < 0 and c > 0 using linearization.
- 4. Can you determine the stability of the equilibrium point x = (0, 0) when c = 0 using linearization? If not, find a suitable Lyapunov function to show that the equilibrium is stable. [Hint: Think pendulum]
- 5. Your friend from EPFL thinks that the equilibrium point x = (0,0) is globally asymptotically stable for c = 1. Explain why this is not the case.

Exercise 4

1	2	3	Exercise
5	10	10	25 Points

Consider the linear system Σ given by:

$$\Sigma: \qquad \ddot{y}(t) + (2 - \alpha)\dot{y}(t) - 2\alpha y(t) = \dot{u}(t) - u(t) \tag{4}$$

where $\alpha \in \mathbb{R}$ is a system parameter.

1. Compute the transfer function G(s) of the system Σ .

Next, consider the system Σ connected to a controller as shown in Figure 2.



Figure 2: Feedback system

- 2. Consider the case $\alpha = -0.01$. Figure 3 shows the Bode diagram of the transfer function G(s) of the system Σ for $\alpha = -0.01$. The maximum of the gain $|G(j\omega)|$ occurs at $\omega = 0$.
 - (a) Compute $|G(j\omega)|$ at $\omega = 0$.
 - (b) Apply the Small gain theorem (corollary of the Bode Stability criterion) to obtain a range for the control gain K for which the feedback system shown in Figure 2 is stable.



Figure 3: Bode diagram of the open-loop transfer function of the system Σ for $\alpha = -0.01$.

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3. Next, consider the case $\alpha = 10$. Figure 4 shows the Nyquist diagram of the transfer function G(s) of the system Σ for $\alpha = 10$. Use the Nyquist stability criterion to show that there does not exist a K for which the closed loop system is stable.

[Hint: Show that the Nyquist criterion is violated both when $\frac{1}{K}$ is encircled by the Nyquist plot and when it is not.]



Figure 4: Nyquist diagram of the open-loop transfer function G(s) of the system Σ for $\alpha = 10$.