

Optimal and Distributed Frequency Control of Transmission Grids

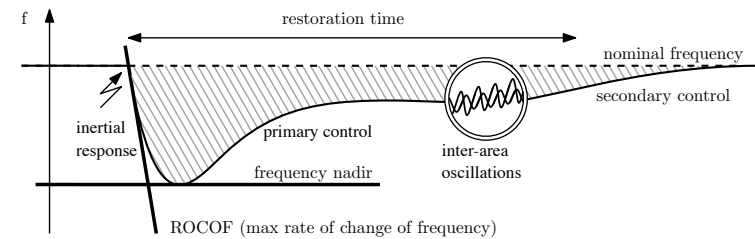
John W. Simpson-Porco



ECC Tutorial Session, Naples, Italy

July 1, 2019

Response to disturbance of an ideal power system

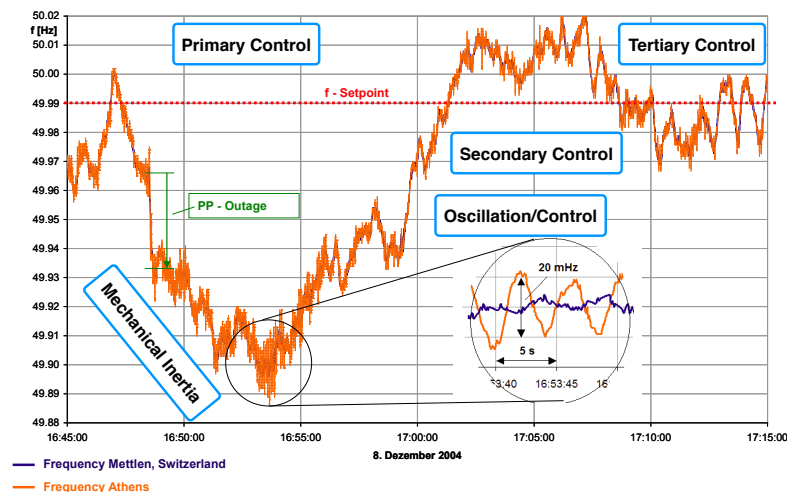


- 1 Physical inertia instantly provides decentralized **derivative** control
- 2 Decentralized *primary loops* at devices provide **proportional** control
- 3 System-wide secondary loop provides centralized **integral** control

Disturbance attenuation

Disturbance rejection

Response to disturbance in a real power system



Source: W. Sattinger, Swissgrid

When secondary frequency control goes wrong . . .

swissgrid

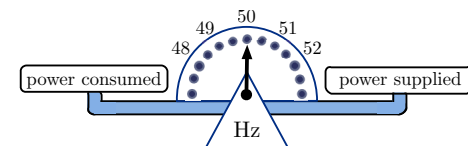
Grid projects About us Customers de fr it en

6 March 2018 | News

Frequency deviation in continental European grid leads to grid time deviations

"The missing energy amounts currently to 113 GWh . . . The decrease . . . is affecting also those electric clocks that are steered by the frequency of the power system . . . they show currently a delay of close to six minutes."

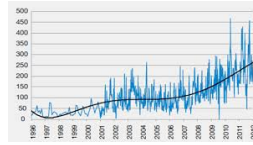
–ENTSO-E Press Release



Modern challenges for control engineers

1 Declining inertia and load-frequency responsiveness

- **Sensitive** system
- **Large** and **frequent** deviations



2 Heterogeneous small-scale power sources

- Many **small** but **fast** sources
- Fast freq. regulation markets

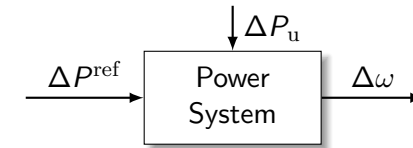


Opportunities for control engineers

- 1 Inverter-based resources and fast communication
- 2 Hierarchical control of **many** small devices

4 / 16

Simple dynamic models for frequency control (single area)



- Control inputs:** Power set-points to devices ΔP_i^{ref}
Meas. / Controlled output: Frequency error $\Delta\omega$
Unknown disturbances: Uncontrolled load/generation $\Delta P_{u,i}$

$$\begin{aligned} \Delta\dot{\theta}_i &= \Delta\omega_i, \\ M_i\Delta\dot{\omega}_i &= -\sum_{j=1}^n T_{ij}(\Delta\theta_i - \Delta\theta_j) - D_i\Delta\omega_i + \Delta P_{m,i} + \Delta P_{u,i} \\ T_i\Delta\dot{P}_{m,i} &= -\Delta P_{m,i} - R_{d,i}^{-1}\Delta\omega_i + \Delta P_i^{\text{ref}}. \end{aligned}$$

(Note: Real governor model may be highly nonlinear!)

5 / 16

Fundamental insights from output regulation theory

Johnson, Davison, Francis, Wonham ...

System models are BIBO stable with steady-state given by

$$\Delta\omega = \underbrace{\beta^{-1}\mathbf{1}\mathbf{1}^T}_{:=G_0 \text{ (DC Gain)}} (\Delta P_u + \Delta P^{\text{ref}}), \quad \beta = \underbrace{\sum_i (D_i + R_{d,i}^{-1})}_{\text{Total proportional gain}}.$$

- 1 **Insight #1:** $\Delta\omega \in \text{span}(\mathbf{1}_n) \iff$ "frequency is global"
- 2 **Insight #2:** Only *sum* of powers matters \implies Resource allocation
- 3 **Insight #3:** $\text{rank}(G_0) = 1$, which means ...

Only **one** frequency integrator permitted in **any** internally stable secondary control system!

6 / 16

Optimal allocation of secondary resources

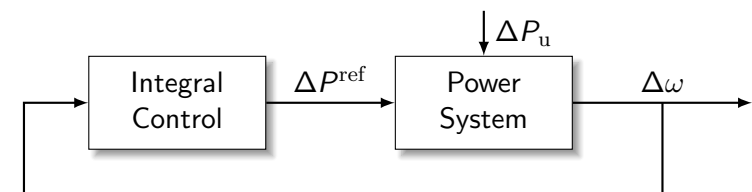
Optimally allocate inputs subject to **power balance** and **limits**

$$\begin{aligned} &\text{minimize} && \sum_{i=1}^n J_i(\Delta P_i^{\text{ref}}) \\ &\text{subject to} && \sum_{i=1}^n \Delta P_i^{\text{ref}} + \Delta P_{u,i} = 0 \\ &&& \Delta P_i^{\text{ref}} \in \{\text{power limits}\}. \end{aligned}$$

Equivalent:

- (i) Power balance
- (ii) Regulation $\Delta\omega = 0$

Solve w/ $\Delta\omega$ feedback + Lagrange coordination



7 / 16

Hierarchical or distributed coordination

First-order **optimality condition**: $\exists \lambda$ s.t. $\forall i \quad \nabla J_i(\Delta P_i^{\text{ref}}) = \lambda$.

How to enforce this **equal marginal cost** condition?

1 Centralized approach:

$$\underbrace{\tau \dot{\eta} = -\Delta \omega_{\text{meas}}}_{\text{Central integral action}}$$

$$\underbrace{\Delta P_i^{\text{ref}} = (\nabla J_i)^{-1}(\eta)}_{\text{Allocation rule}}$$

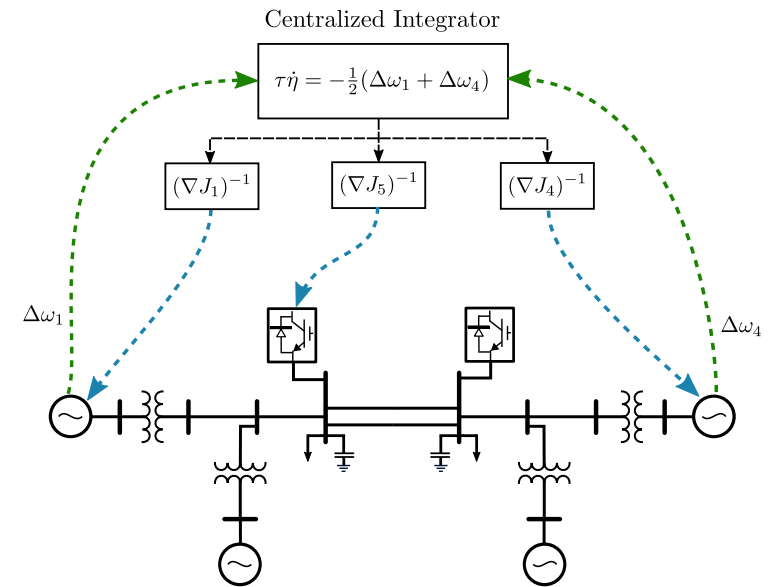
2 Distributed approach (consensus version):

$$\underbrace{\tau_i \dot{\eta}_i = -\Delta \omega_i - \sum_{j=1}^n a_{ij}(\eta_i - \eta_j)}_{\text{Distributed integral action}}$$

$$\underbrace{\Delta P_i^{\text{ref}} = (\nabla J_i)^{-1}(\eta_i)}_{\text{Allocation rule}}$$

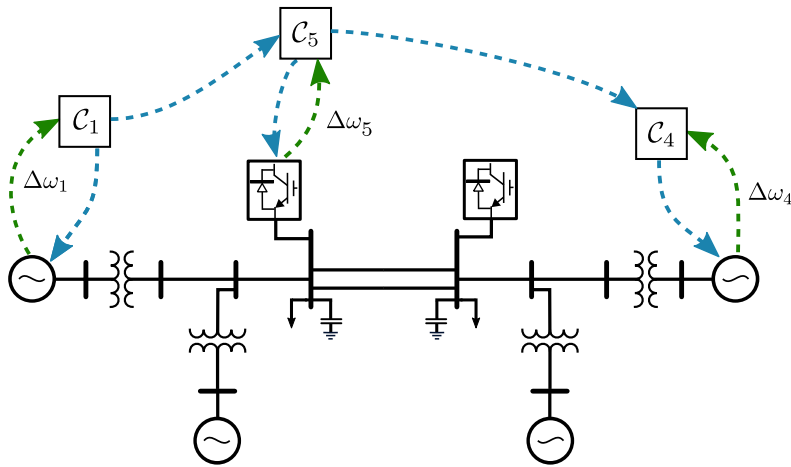
8 / 16

Centralized architecture



9 / 16

Distributed architecture

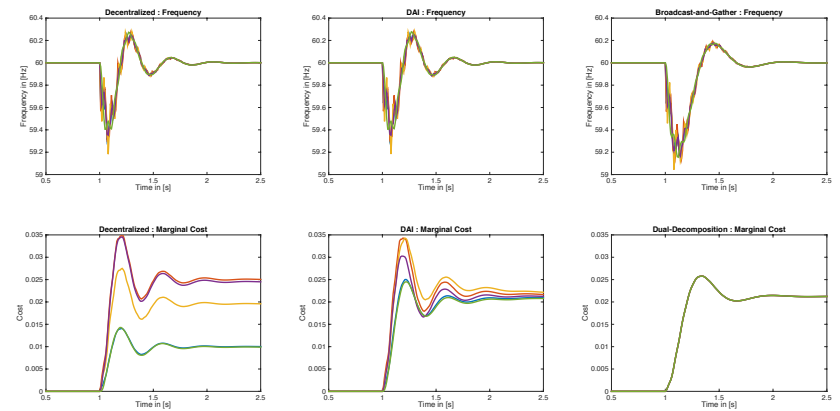


- Communication graph has a globally reachable node (nec. & suff.)

10 / 16

Distributed vs. centralized

Simulation on New England 39 Bus System¹



¹F. Dörfler and S. Grammatico, "Gather-and-broadcast frequency control in power systems," *Automatica*, 2017.

11 / 16

Hierarchical or distributed coordination contd.

③ **Distributed** approach (primal-dual version) uses

- **virtual** phase angles $\hat{\theta}$
- **virtual flow** on line $\ell = (i, j)$ as $\hat{p}_\ell = T_\ell(\hat{\theta}_i - \hat{\theta}_j)$

$$\begin{aligned} & \text{minimize} && \sum_{i=1}^n J_i(\Delta P_i^{\text{ref}}) + \frac{1}{2} D_i (\Delta \omega_i)^2 \\ & \text{subject to} && \Delta P_{u,i} + \Delta P_i^{\text{ref}} - D_i \Delta \omega_i = \sum_j A_{i\ell} \hat{p}_\ell \\ & && \Delta P_{u,i} + \Delta P_i^{\text{ref}} = \sum_j T_{ij}(\hat{\theta}_i - \hat{\theta}_j) \end{aligned}$$

Now apply primal-descent and dual-ascent to **Lagrangian** \mathcal{L}

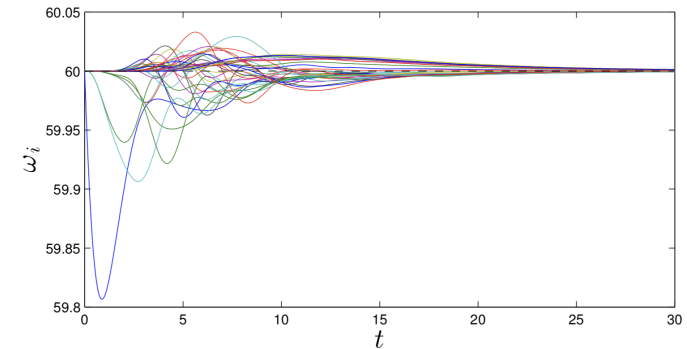
Primal dynamics: Embeds natural system dynamics

Dual dynamics: Distributed control

12 / 16

Primal-dual method

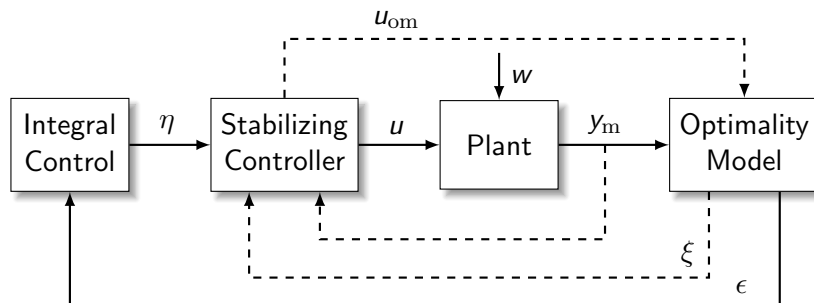
Simulation on New England 39 Bus System²



²E. Mallada and C. Zhao and S. Low, "Optimal Load-Side Control for Frequency Regulation . . ." *IEEE TAC*, 2017.

13 / 16

Unifying perspective: Optimal Steady-State Control³



Optimality Model: creates optimality error signal ϵ

Integral Control: integrates error ϵ

Stabilizing Controller: stabilizes closed-loop system

³L. Lawrence, JWSP, E. Mallada "Linear-convex optimal steady-state control," *TAC*, Submitted.

14 / 16

Practical challenges

We have discussed **structural and architectural** aspects, but . . .

- ① Dynamic models are **highly** uncertain and time-varying
 - Device models often either unknown or not maintained
 - High-order governor models, deadbands, saturation all important
 - Machines dispatched in and out of system every ≈ 15 mins
 - Load characteristics change dramatically day-to-day
 - Even DC gain (β^{-1}) of system can vary by a factor of 2–3!

Possible approach: **data-driven** + **gain-scheduled** methods

- ② Communication infrastructure challenges
 - If it ain't broke, don't upgrade it
 - High-bandwidth control over comm. channels perceived as risky

15 / 16

Questions



<https://ece.uwaterloo.ca/~jwsimpso/>
jwsimpson@uwaterloo.ca