Cyber-Physical Systems under Attack

Models, Fundamental Limitations, and Monitor Design

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Many critical infrastructures are cyber-physical systems:

- power generation and distribution networks
- water networks and mass transportation systems
- econometric models (W. Leontief, Input output economics, 1986)

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sensor networks

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• energy-efficient buildings (heat transfer)

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Security and Reliability of Cyber-Physical Systems

Cyber-physical security is a fundamental obstacle

challenging the smart grid vision.

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Wa	er supply networks are among the nation's most critical infrastructures						
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S. Amin, X. Litrico, S.S. Sastry, and A.M. Bayen. "Stealthy Deception Attacks on Water SCADA Systems" ACM International Conference on Hybrid systems. 2010.

A Simple Example: WECC 3-machine 6-bus System



$ \begin{array}{c} & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & $

- **O Physical dynamics:** classical generator model & DC load flow
- **2** Measurements: angle and frequency of generator g_1
- Attack: modify real power injections at buses b₄ & b₅
 "Distributed internet-based load altering attacks against smart power grids" IEEE Trans on Smart Grid, 2011

The attack affects the second and third generators while remaining undetected from measurements at the first generator

From Fault Detection and Cyber Security to Cyber-Physical Security

Cyber-physical security exploits system dynamics to assess correctness of measurements, and compatibility of measurement equation

Cyber-physical security extends classical fault detection, and complements/augments cyber security

- classical fault detection considers only *generic* failures, while cyber-physical attacks are worst-case attacks
- cyber security does not exploit compatibility of measurement data with physics/dynamics
- cyber security methods are ineffective against attacks that affect the physics/dynamics

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Models of Cyber-physical Systems: Water Networks

Linearized municipal water supply network model:

- reservoirs with constant pressure heads: $h_i(t) = h_i^{\text{reservoir}} = const.$
- ⁽²⁾ pipe flows obey linearized Hazen-Williams eq: $Q_{ij} = g_{ij} \cdot (h_i h_j)$
- **3** balance at tank: $A_i \dot{h}_i = \sum_{j \to i} Q_{ji} - \sum_{i \to k} Q_{ik}$
- demand = balance at junction: $d_i = \sum_{j \to i} Q_{ji} - \sum_{i \to k} Q_{ik}$



 \Rightarrow Linear differential-algebraic dynamics: $E\dot{x} = Ax$

Models of Cyber-Physical Systems: Power Networks

Small-signal structure-preserving power network model:

 transmission network: generators ■, buses ●, DC load flow assumptions, and network susceptance matrix Y = Y^T



generators modeled by swing equations:

$$M_i \ddot{ heta}_i + D_i \dot{ heta}_i = P_{\mathsf{mech.in},i} - \sum_j Y_{ij} \cdot (heta_i - heta_j)$$

Solution State State

$$0 = P_{\mathsf{load},i} - \sum_{j} Y_{ij} \cdot \left(heta_i - heta_j
ight)$$



- \Rightarrow Linear differential-algebraic dynamics: $E\dot{x} = Ax$
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Models for Attackers and Security System

Byzantine Cyber-Physical Attackers

- colluding omniscent attackers:
 - know model structure and parameters
 - measure full state
 - perform unbounded computation
 - ${\scriptstyle \bullet }$ can apply some control signal and corrupt some measurements
- 2 attacker's objective is to change/disrupt the physical state

Security System

- knows structure and parameters
- 2 measures output signal
- **③** security systems's objective is to detect and identify attack

() characterize fundamental limitations on security system

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2 design filters for detectable and identifiable attacks

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Model of Cyber-Physical Systems under Attack

- **O Physics** obey linear differential-algebraic dynamics: $E\dot{x}(t) = Ax(t)$
- **2** Measurements are in continuous-time: y(t) = Cx(t)
- Oppose Cyber-physical attacks are modeled as unknown input u(t) with unknown input matrices B & D

 $E\dot{x}(t) = Ax(t) + Bu(t)$ y(t) = Cx(t) + Du(t)

This model includes **genuine faults** of system components, **physical attacks**, and **cyber attacks** caused by an omniscient malicious intruder.

Q: Is the attack (B, D, u(t)) detectable/identifiable from the output y(t)?

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Prototypical Attacks

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Related Results on Cyber-Physical Security

- Par	angletti, E. Dönfler, E. Bullo, Culton Dhuring, Sustanna Under Attack, Security, Seminar UCLA, 13					
	Our framework includes and generalizes most of these results					
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Technical Assumptions

$$E\dot{x}(t) = Ax(t) + B_K u_K(t)$$

 $y(t) = Cx(t) + D_K u_K(t)$

Technical assumptions guaranteeing existence, uniqueness, & smoothness:

- (i) (E, A) is regular: |sE A| does not vanish for all $s \in \mathbb{C}$
- (ii) the initial condition x(0) is consistent (can be relaxed)
- (iii) the unknown input $u_{\mathcal{K}}(t)$ is sufficiently smooth (can be relaxed)

• Attack set K = sparsity pattern of attack input

An attack remains undetected if its effect on measurements is undistinguishable from the effect of some nominal operating conditions



Definition (Undetectable attack set)

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The attack set K is *undetectable* if there exist initial conditions x_1, x_2 , and an attack mode $u_K(t)$ such that, for all times t

$$y(x_1, u_K, t) = y(x_2, 0, t)$$

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By linearity, an undetectable attack is such that $y(x_1 - x_2, u_K, t) = 0$ • zero dynamics of input/output system

Theorem

For the attack set K, there exists an undetectable attack if and only if

$$\begin{bmatrix} sE - A & -B_K \\ C & D_K \end{bmatrix} \begin{bmatrix} x \\ g \end{bmatrix} = 0$$

for some s,
$$x \neq 0$$
, and g.

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Undetectability of Replay Attacks



1 two attack channels: \bar{u}_K , u_K

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2
$$\operatorname{Im}(C) \subseteq \operatorname{Im}(D_K)$$

3 $B_K \neq 0$

Undetectability follows from solvability of

$$\begin{bmatrix} sE - A & -B_K & 0 \\ C & 0 & D_K \end{bmatrix} \begin{bmatrix} x \\ g_1 \\ g_2 \end{bmatrix} = 0$$

- $x = (sE A)^{-1}B_{K}g_{1}, g_{2} = D_{K}^{\dagger}C(sE A)^{-1}B_{K}g_{1}$
- replay attacks can be detected though *active detectors*
- replay attacks are not worst-case attacks

Unidentifiable Attack Definition

The attack set K remains unidentified if its effect on measurements is undistinguishable from an attack generated by a distinct attack set $R \neq K$

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Definition (Unidentifiable attack set)

The attack set K is *unidentifiable* if there exists an admissible attack set $R \neq K$ such that

$$y(x_K, u_K, t) = y(x_R, u_R, t).$$

• an undetectable attack set is also unidentifiable

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Unidentifiable Attack

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By linearity, the attack set K is unidentifiable if and only if there exists a distinct set $R \neq K$ such that $y(x_K - x_R, u_K - u_R, t) = 0$.

Theorem

For the attack set K, there exists an unidentifiable attack if and only if

$$\begin{bmatrix} sE - A & -B_K & -B_R \\ C & D_K & D_R \end{bmatrix} \begin{bmatrix} x \\ g_K \\ g_R \end{bmatrix} = 0$$

for some s, $x \neq 0$, g_K , and g_R .

So far we have shown:

- fundamental detection/identification limitations
- system-theoretic conditions for undetectable/unidentifiable attacks

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From Algebraic to Graph-theoretical Conditions





- the vertex set is the union of the state, input, and output variables
- edges corresponds to nonzero entries in E, A, B, C, and D
- system theoretic properties expressed through graph theoretic notions





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- **O Physical dynamics:** classical generator model & DC load flow
- **2** Measurements: angle and frequency of generator g_1
- **3** Attack: modified real power injections at buses $b_4 \& b_5$

The attack through b_4 and b_5 excites only zero dynamics for the measurements at the first generator

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Zero Dynamics and Connectivity

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A linking between two sets of vertices is a set of mutually-disjoint directed paths between nodes in the sets



Theorem (Detectability, identifiability, linkings, and connectivity)

If the maximum size of an input-output linking is k:

- there exists an undetectable attack set K_1 , with $|K_1| \ge k$, and
- there exists an unidentifiable attack set K_2 , with $|K_2| \ge \lceil \frac{k}{2} \rceil$.
- statement becomes necessary with *generic* parameters
- statement applies to systems with parameters in polytopes

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WECC 3-machine 6-bus System Revisited



Decentralized Monitor Design

Partition the physical system with geographically deployed control centers:



- (i) control center *i* knows E_i , A_i , and C_i , and neighboring A_{ij}
- (ii) control center *i* can communicate with control center $j \Leftrightarrow A_{ji} \neq 0$
- (iii) E&C are blockdiagonal, (E_i, A_i) is regular $\& (E_i, A_i, C_i)$ is observable

Centralized Detection Monitor Design

System under attack (B, D, u(t)):

 $E\dot{x}(t) = Ax(t) + Bu(t)$

y(t) = Cx(t) + Du(t)

Proposed centralized detection filter:

$$E\dot{w}(t) = (A + GC)w(t) - Gy(t)$$

 $r(t) = Cw(t) - y(t)$

Theorem (Centralized Attack Detection Filter)

Assume w(0) = x(0), (E, A + GC) is Hurwitz, and attack is detectable. Then r(t) = 0 if and only if u(t) = 0.

- \bigcirc the design is independent of *B*, *D*, and u(t)
- \odot if $w(0) \neq x(0)$, then asymptotic convergence
- © a direct centralized implementation may not be feasible due to high dimensionality, spatial distribution, communication complexity, ...

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Decentralized Monitor Design: Continuous Communication

System under attack: Decentralized detection filter:

$$E\dot{x}(t) = Ax(t) + Bu(t) \qquad E$$
$$y(t) = Cx(t) + Du(t)$$

 $E\dot{w}(t) = (A_D + GC)w(t) + A_Cw(t) - Gy(t)$ r(t) = Cw(t) - y(t)

where $A = A_D + A_C$

where $G = \text{blkdiag}(G_1, \ldots, G_N)$

Theorem (Decentralized Attack Detection Filter)

Assume that w(0) = x(0), $(E, A_D + GC)$ is Hurwitz, and

$$ho\left((j\omega E - A_D - GC)^{-1}A_C\right) < 1$$
 for all $\omega \in \mathbb{R}$.

If the attack is detectable, then r(t) = 0 if and only if u(t) = 0.

 $\ensuremath{\textcircled{\ensuremath{\textcircled{}}}}$ the design is decentralized but achieves centralized performance

© the design requires continuous communication among control centers

Digression: Gauss-Jacobi Waveform Relaxation

• Standard Gauss-Jacobi relaxation to solve a linear system Ax = u:

$$x_{i}^{(k)} = \frac{1}{a_{ii}} \left(u_{i} - \sum_{j \neq i} a_{ij} x_{j}^{(k-1)} \right) \quad \Leftrightarrow \quad x^{(k)} = -A_{D}^{-1} A_{C} x^{(k-1)} + A_{D}^{-1} u$$

Convergence:
$$\lim_{k \to \infty} x^{(k)} \to x = A^{-1} u \quad \Leftrightarrow \quad \rho(A_{D}^{-1} A_{C}) < 1$$

• Gauss-Jacobi waveform relaxation to solve $E\dot{x}(t) = Ax(t) + Bu(t)$:

$$E\dot{x}^{(k)}(t) = A_D x^{(k)}(t) + A_C x^{(k-1)}(t) + Bu(t), \quad t \in [0, T]$$

Convergence for (E, A) Hurwitz & u(t) integrable in $t \in [0, T]$:

 $\lim_{k\to\infty} x^{(k)}(t) \to x(t) \quad \Leftarrow \quad \rho\left((j\omega E - A_D)^{-1}A_C\right) < 1 \quad \forall \, \omega \in \mathbb{R}$

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Implementation of Distributed Attack Detection Filter

Distributed iterative procedure to compute the residual r(t), $t \in [0, T]$:

- set k := k + 1, and compute w_i^(k)(t), t ∈ [0, T], by integrating

 E_iw_i^(k)(t) = (A_i + G_iC_i)w_i^(k)(t) + ∑_{j≠i} A_{ij}w_j^(k-1)(t) G_iy_i(t)
 transmit w_i^(k)(t) to control center j if A_{ij} ≠ 0
 update w_i^(k)(t) with the signal received from control center j
- \Rightarrow For k sufficiently large, $r_i^{(k)}(t) = C_i w_i^{(k)}(t) y_i(t) \approx 0 \Leftrightarrow$ no attack
- \Rightarrow Receding horizon implementation: move integration window [0, T]
- \Rightarrow Distributed verification of convergence cond.: $\rho(\cdot) < 1 \iff \|\cdot\|_{\infty} < 1$.

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Distributed Monitor Design: Discrete Communication

Distributed attack detection filter:

$$E\dot{w}^{(k)}(t) = (A_D + GC)w^{(k)}(t) + A_Cw^{(k-1)}(t) - Gy(t)$$
$$r^{(k)}(t) = Cw^{(k)}(t) - y(t)$$

where $G = \text{blkdiag}(G_1, \ldots, G_N)$, $t \in [0, T]$, and $k \in \mathbb{N}$

Theorem (Distributed Attack Detection Filter)

Assume that $w^{(k)}(0) = x(0)$ for all $k \in \mathbb{N}$, y(t) is integrable for $t \in [0, T]$, $(E, A_D + GC)$ is Hurwitz, and

$$ho\left((j\omega \mathsf{E}-\mathsf{A}_D-\mathsf{GC})^{-1}\mathsf{A}_{\mathsf{C}}
ight)<1 \quad ext{ for all }\omega\in\mathbb{R}\,.$$

If the attack is detectable, then $\lim_{k\to\infty} r^{(k)}(t) = 0$ if and only if u(t) = 0 for all $t \in [0, T]$.

An Illustrative Example: IEEE 118 Bus System

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Convergence of waveform relaxation:



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- **Physics:** classical generator model and DC load flow model
- Measurements: generator angles
- Attack of all measurements in Area 1

Residuals $r_i^{(k)}(t)$ for k = 100:



Centralized Identification Monitor Design

System under attack $(B_K, D_K, u_K(t))$:

Centralized identification filter:

 $\bar{E}\dot{w}(t) = \bar{A}w(t) - \bar{G}y(t)$

 $r_{\mathcal{K}}(t) = MCw(t) - Hy(t)$

$$E\dot{x}(t) = Ax(t) + \frac{B_{K}u_{K}(t)}{B_{K}u_{K}(t)} + \frac{B_{R}u_{R}(t)}{B_{K}u_{K}(t)}$$
$$y(t) = Cx(t) + \frac{D_{K}u_{K}(t)}{B_{K}u_{K}(t)} + \frac{B_{R}u_{R}(t)}{B_{K}u_{K}(t)}$$

• only $u_K(t)$ is active, i.e., $u_R(t) = 0$ at all times

Theorem

Assume w(0) = x(0), and attack set is identifiable. Then $r_K(t) = 0$ if and only if K is the attack set.

- \bigcirc if $w(0) \neq x(0)$, then asymptotic convergence
- © a direct centralized implementation may not be feasible
- \odot design depends on $(B_K, D_K) \Rightarrow$ combinatorial complexity (NP-hard)

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Distributed Monitor Design

Partition the physical system with geographically deployed control centers:



- (i) control center *i* knows E_i , A_i , and C_i , and neighbouring A_{ii}
- (ii) control center *i* can communicate with control center $j \Leftrightarrow A_{ii} \neq 0$
- (iii) E&C are blockdiagonal, (E_i, A_i) is regular & (E_i, A_i, C_i) is observable

Design Method Controlled, Conditioned, and Deflating Subspaces



Let \mathcal{S}^*_{κ} be the smallest subspace of the state space such that

• $\exists G$ such that $(A + GC)S_{K}^{*} \subseteq S_{K}^{*}$ and $\mathcal{R}(B_{K} + GD_{K}) \subseteq S_{K}^{*}$

Design steps:

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- 1) compute smallest conditioned invariant subspace $\mathcal{S}_{\mathcal{K}}^*$
- 2) make the subspace \mathcal{S}_{K}^{*} invariant by output injection
- 3) build a residual generator for the quotient space $\mathcal{X} \setminus \mathcal{S}_{K}^{*}$
- 4) the residual is not affected by $u_{\mathcal{K}}(t)$

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Distributed Attack Identification: a Naive Solution



- Known area dynamics
- Onknown connection inputs
- Unknown input attacks

Consider unknown interconnection inputs as attacks and design attack detection and identification monitors as in the centralized case.

- completely distributed the design
- © very low combinatorics
- © no communication among different areas
- © solvability conditions are very strict (boundary attacks)

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Distributed Attack ID: a Divide & Conquer Solution

- **1** Treat the connection inputs as unknown
- 2 Reconstruct the state (modulo \mathcal{V}) of area via unknown-input observer
- ${\small \textcircled{\sc 0}}$ Communicate estimate and ${\small \mathcal{V}}$ to neighboring areas

The unknown part of the connection input is restricted to $\ensuremath{\mathcal{V}}.$



A Case Study: RTS-96 Bus System



- **O Physical dynamics:** classical generator model & DC load flow
- **2** Measurements: angle and frequency of all generators
- **3** Attack: modify governor control at generators $g_{101} \& g_{102}$
- **OMONITORS:** our centralized detection and identification filters

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An Example of Distributed Attack Identification



- $\ensuremath{\textcircled{}}$ completely distributed the design
- ③ very low combinatorics

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- $\ensuremath{\textcircled{}}$ little communication among different areas
- $\ensuremath{\textcircled{}}$ solvability conditions are easier to verify

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RTS-96 Bus System: Linear Dynamics without Noise



- x(t): generators trajectories
- r(t): detection residual
- $r_{\kappa}(t)$: identification residual for K

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- $r_R(t)$: identification residual for R
- filters are designed via conditioned invariance technique

RTS-96 Bus System: Linear Dynamics with Noise

RTS-96 Bus System: Nonlinear Dynamics

- x(t)MMM 15.5 0 r(t)-0.1 14.5 10 20 15.5 15 15 $r_K(t)$ 15 20 15.5 $r_R(t)$ 14.5 20 15 !
- x(t): generators trajectories ۲

r(t): detection residual

- $r_{K}(t)$: identification residual for K
- $r_R(t)$: identification residual for R
- filters are designed via conditioned invariance and Kalman gain



- x(t): generators trajectories
- r(t): detection residual
- $r_{K}(t)$: identification residual for K
- $r_R(t)$: identification residual for R
- filters are designed via conditioned invariance and Kalman gain

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Conclusion

We have presented:

- a modeling framework for cyber-physical systems under attack
- 2 fundamental detection and identification limitations
- System- and graph-theoretic detection and identification conditions
- Gentralized attack detection and identification procedures
- Idistributed attack detection and identification procedures

Ongoing and future work:

- Optimal network partitioning for distributed procedures
- effect of noise, modeling uncertainties & communication constraints
- **9** quantitative analysis of **cost** and **effect** of attacks
- applications to distributed-parameters cyber-physical systems

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A Case Study: Competitive Power Generation Environment

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A Case Study: Competitive Power Generation Environment

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- malicious coalition: K = {1,9} (PacNW) with sacrificial machine {9}
- control minimizes $\|\omega_9(t)\|_{\mathcal{L}_{\infty}}$ subject to $\|\omega_{16}(t)\|_{\mathcal{L}_{\infty}} \ge 1$ (Utah)
- $\Rightarrow\,$ non-colluding generators will be damaged





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Western North American Grid



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Our geometric control methods can also be used for attack design.



Western North American Power Grid

- scenario: a subset of utility companies *K* form a coalition
- **goal:** disrupt the power generation of competitors
- strategy: choose K* ⊂ K sacrificial generators and design an input not affecting K \ K* while maximizing damage at non-colluding generators
- additionally here: design such that impact on K^* is minimal

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