Virtual Inertia Emulation and Placement in Power Grids

Optimization & Control for Tomorrow's Power Systems (ECC'16)

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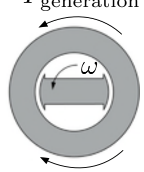
HORIZON 2020

At the beginning of power systems was ...

At the beginning was the **synchronous machine**:

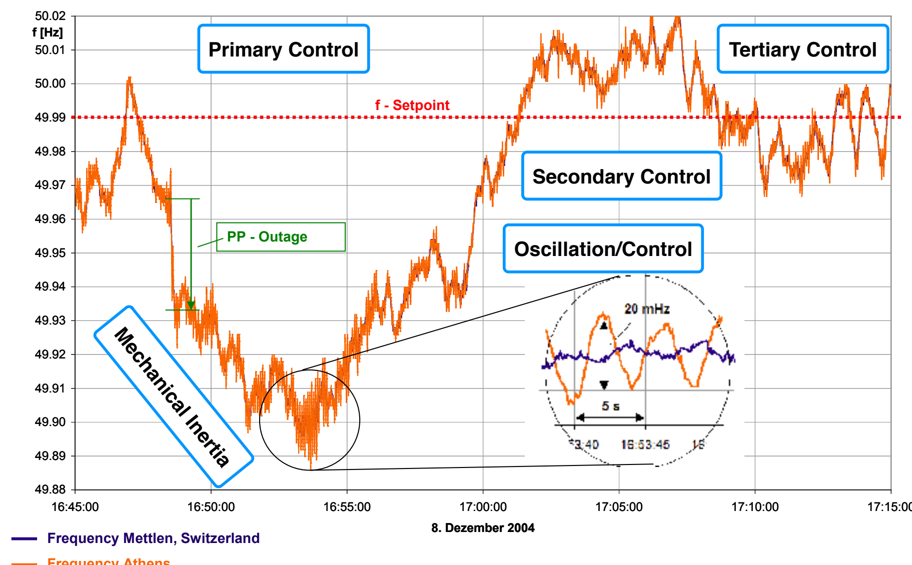
$$M \frac{d}{dt}\omega(t) = P_{\text{generation}}(t) - P_{\text{demand}}(t)$$

change of kinetic energy = instantaneous power balance



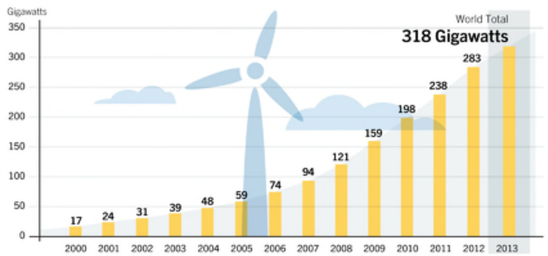
Fact: the AC grid & all of power system operation has been designed around synchronous machines.

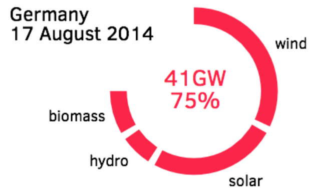
Operation centered around bulk synchronous generation

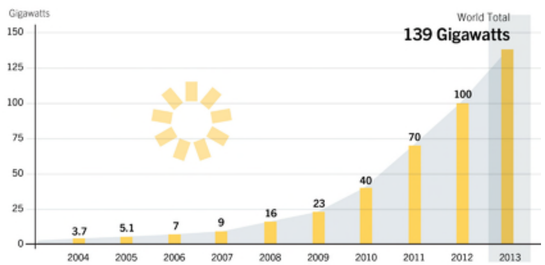


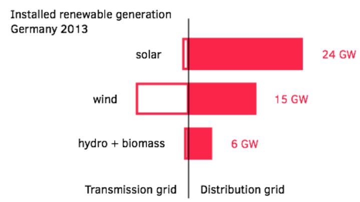
Source: W. Sattinger, Swissgrid

Distributed/non-rotational/renewable generation on the rise









Source: Renewables 2014 Global Status Report

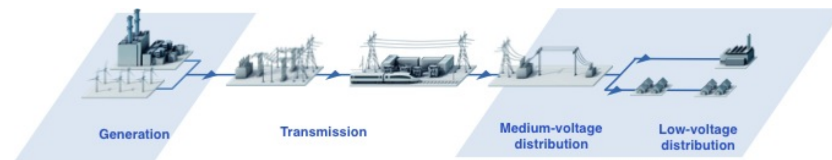
A few (of many) game changers ...

synchronous generator

new workhorse

scaling

location & distributed implementation



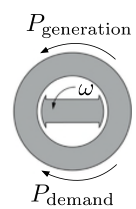
Almost all operational problems can principally be resolved ... **but one (?)**

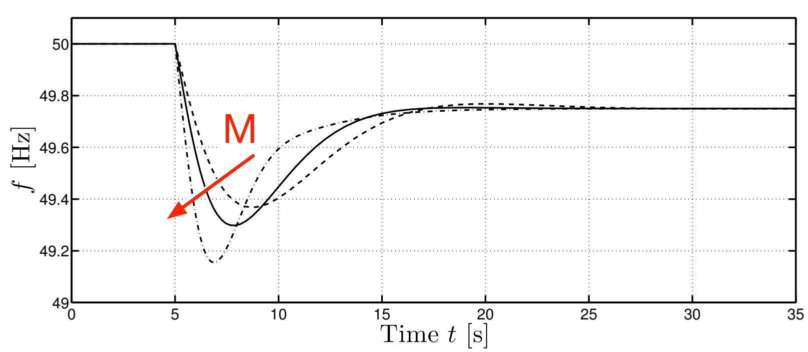
Fundamental challenge: operation of low-inertia systems

We slowly loose our giant electromechanical low-pass filter:

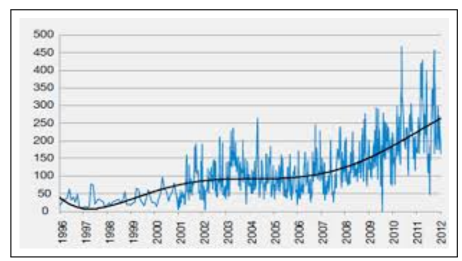
$$\mathbf{M}\,\frac{d}{dt}\,\omega(t) \;=\; P_{\text{generation}}(t) - P_{\text{demand}}(t)$$

change of kinetic energy = instantaneous power balance

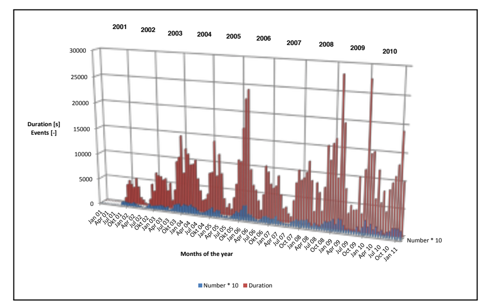




Low-inertia stability: # 1 problem of distributed generation



frequency violations in Nordic grid (source: ENTSO-E)



same in Switzerland (source: Swissgrid)

inertia is shrinking, time-varying, & localized, ... & increasing disturbances

Solutions in sight: none really ... other than **emulating virtual inertia** through fly-wheels, batteries, super caps, HVDC, demand-response, ...

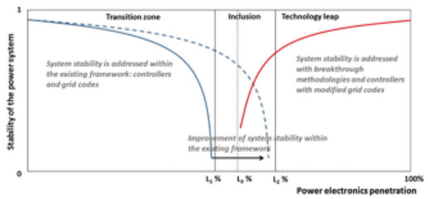
Low inertia issues have been broadly recognized

by TSOs, device manufacturers, academia, funding managers, etc.

Massive **I**nte**GRAT**ion of power **E**lectronic devices

"The question that has to be examined is: how much power electronics can the grid cope with?" (European Commission)

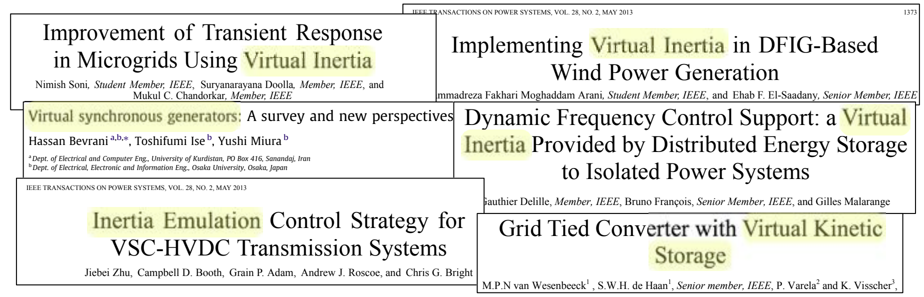
current controls **what else?**



all options are on the table and keep us busy . . .

Virtual inertia emulation

devices commercially available, required by grid-codes, or incentivized through markets


Improvement of Transient Response in Microgrids Using Virtual Inertia
Nimish Soni, Student Member, IEEE, Suryanarayana Doolla, Member, IEEE, and Mukul C. Chandorkar, Member, IEEE

IEEE TRANSACTIONS ON POWER SYSTEMS, VOL. 28, NO. 2, MAY 2013
Implementing Virtual Inertia in DFIG-Based Wind Power Generation
...mmadreza Fakhari Moghaddam Arani, Student Member, IEEE, and Ehab F. El-Saadany, Senior Member, IEEE

Virtual synchronous generators: A survey and new perspectives
Hassan Bevrani, Toshifumi Ise, Yushi Miura

Dynamic Frequency Control Support: a Virtual Inertia Provided by Distributed Energy Storage to Isolated Power Systems
...authier Delille, Member, IEEE, Bruno François, Senior Member, IEEE, and Gilles Malarange

IEEE TRANSACTIONS ON POWER SYSTEMS, VOL. 28, NO. 2, MAY 2013
Inertia Emulation Control Strategy for VSC-HVDC Transmission Systems
Jiebei Zhu, Campbell D. Booth, Grain P. Adam, Andrew J. Roscoe, and Chris G. Bright

Grid Tied Converter with Virtual Kinetic Storage
M.P.N van Wesenbeeck, S.W.H. de Haan, Senior member, IEEE, P. Varela and K. Visscher

$$\mathbf{M}\,\frac{d}{dt}\omega(t) \;=\; P_{\text{generation}}(t) - P_{\text{demand}}(t) \;\approx\; \textbf{derivative control on } \omega(t)$$

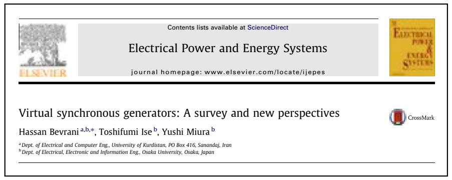
⇒ **open Q's**: which devices? when to do it? who pays?

⇒ **focus today:** **where** to do it? **how** to do it **properly**?

Outline

inertia emulation

Challenges in power converter implementations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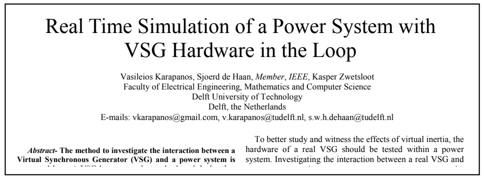
Virtual synchronous generators: A survey and new perspectives

Hassan Bevrani[a,b,*], Toshifumi Ise[b], Yushi Miura[b]


Real Time Simulation of a Power System with VSG Hardware in the Loop

Vasileios Karapanos, Sjoerd de Haan, Member, IEEE, Kasper Zwetsloot

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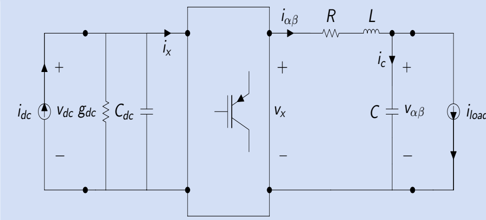
1. **delays** in measurement acquisition, signal processing, & actuation
2. **accuracy** in AC measurements (need averaging)
3. **constraints** on currents, voltages, power, etc.
4. **certificates** on stability, robustness, & performance

today: use DC measurement, exploit analog storage, & passive control

Averaged inverter model



DC cap & AC filter equations:

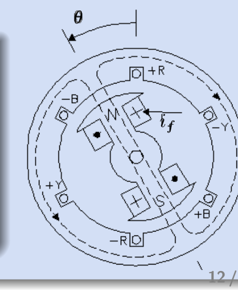
$$C_{dc}\dot v_{dc} = -G_{dc}v_{dc} + i_{dc} - \frac{1}{2}m^\top i_{\alpha\beta}$$
$$C\dot v_{\alpha\beta} = -i_{load} + i_{\alpha\beta}$$
$$L\dot i_{\alpha\beta} = -Ri_{\alpha\beta} + \frac{1}{2}m v_{dc} - v_{\alpha\beta}$$

modulation: $i_x = \frac{1}{2}m^\top i_{\alpha\beta}$, $v_x = \frac{1}{2}m v_{dc}$

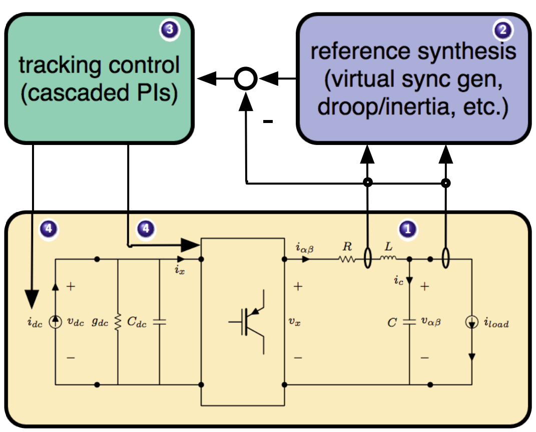
passive: $(i_{dc}, i_{load}) \to (v_{dc}, v_{\alpha\beta})$

model of a synchronous generator

$$\dot\theta = \omega$$
$$M\dot\omega = -D\omega + \tau_m + i_{\alpha\beta}^\top L_m i_f \begin{bmatrix}-\sin(\theta)\\ \cos(\theta)\end{bmatrix}$$
$$C\dot v_{\alpha\beta} = -G_{load}v_{\alpha\beta} + i_{\alpha\beta}$$
$$L_s\dot i_{\alpha\beta} = -Ri_{\alpha\beta} - v_{\alpha\beta} - \omega L_m i_f \begin{bmatrix}-\sin(\theta)\\ \cos(\theta)\end{bmatrix}$$



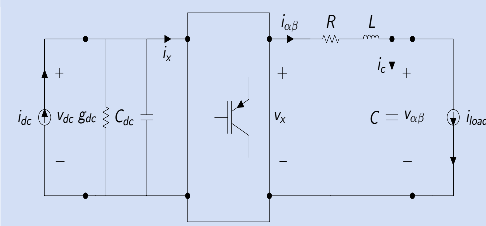
Standard power electronics control would continue by



1. acquiring & processing of **AC measurements**
2. synthesis of **references** (voltage/current/power)
3. **track** references at converter terminals
4. **actuation** via emulation (inner loop) and/or via DC source (outer loop)

let's do **something different** (smarter?) today ...

See the similarities & the differences ?



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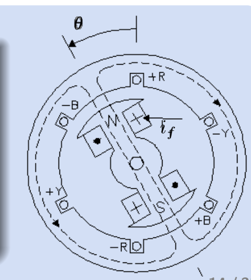
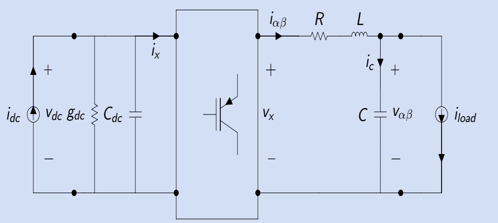


Model matching (≠ emulation) as inner control loop



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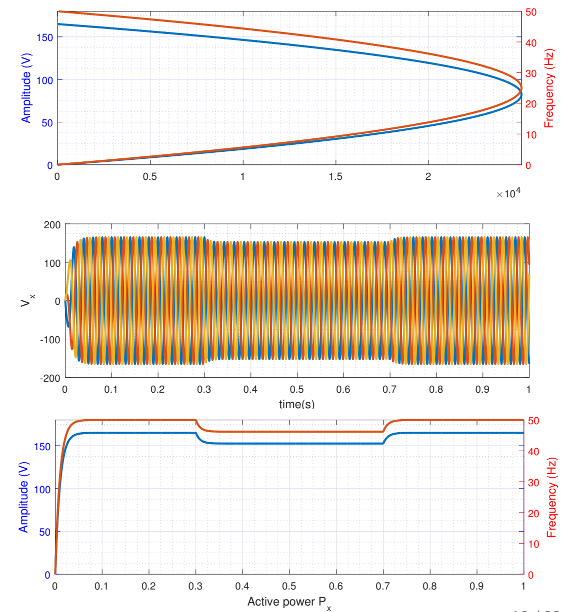
matching control: $\dot{\theta} = \eta \cdot v_{dc}\ ,\ m = \mu \cdot \begin{bmatrix} -\sin(\theta) \\ \cos(\theta) \end{bmatrix}$ with $\eta, \mu > 0$

⇒ **pros:** is balanced, uses natural storage, & based on DC measurement

⇒ **virtual machine** with $M = \frac{C_{dc}}{\eta^2}$, $D = \frac{G_{dc}}{\eta^2}$, $\tau_m = \frac{i_{dc}}{\eta}$, $i_f = \frac{\mu}{\eta L_m}$

Properties of machine matching control

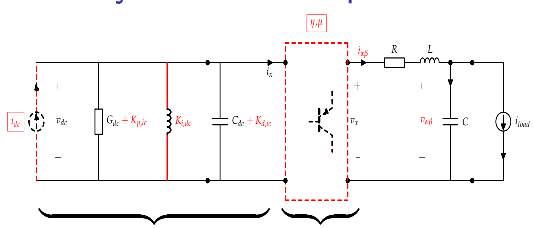
1. quadratic **nose curves**: stationary P vs. $(|V|, \omega)$
   - ⇒ $P \leq P_{\max} = i_{dc}^2/4G_{dc}$
   - ⇒ (P, ω)-**droop** $\approx 1/\eta$
   - ⇒ $(P, |V|)$-**droop** $\approx 1/\mu$
2. remains **passive**: $(i_{dc}, i_{load}) \to (v_{dc}, v_{\alpha\beta})$
3. same **stability condition** as for generators: *supply* $\leq$ *transmission* + *losses*



Machine matching control is only the inner loop

1. solid **plug-and-play** base for outer control loops via i_{dc}, η, & μ inputs

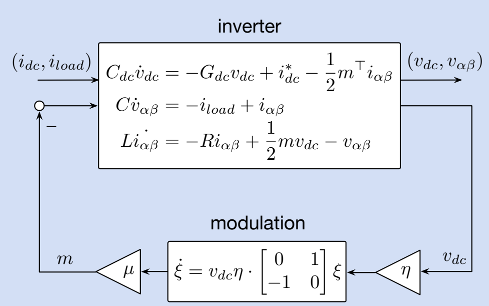
   (e.g., virtual governor, PSS, AVR, synthetic inertia, etc.)



PID on i_{dc} (droop/inertia) or PSS/AVR via μ

2. reformulation as virtual & adaptive **oscillator**

   (c.f., proportional-resonant control or virtual oscillator control strategies)



optimal inertia placement

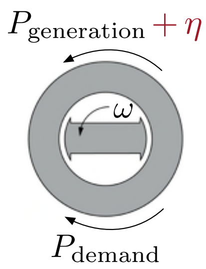
Network swing equation model

$m_i \ddot{\theta}_i + d_i \dot{\theta}_i = p_{in,i} - p_{e,i}$

generator swing equations

$p_{e,i} \approx \sum_{j \in \mathcal{N}} b_{ij}(\theta_i - \theta_j)$

linearized power flows



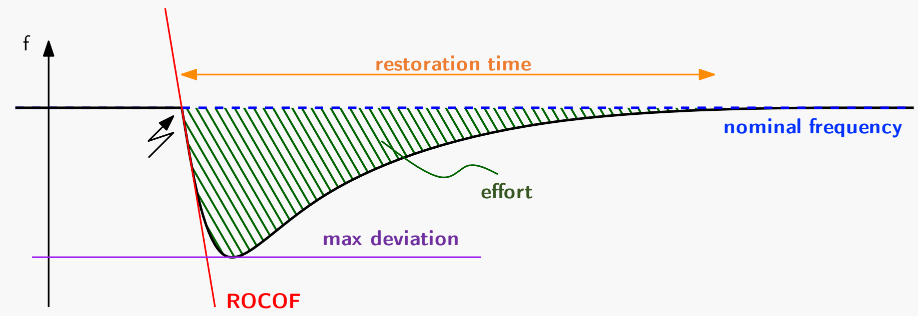
likelihood of **disturbance** at $\#i$: $t_i \geq 0$

state space representation:

$$\begin{bmatrix} \dot{\theta} \\ \dot{\omega} \end{bmatrix} = \underbrace{\begin{bmatrix} 0 & I \\ -M^{-1}L & -M^{-1}D \end{bmatrix}}_{A} \begin{bmatrix} \theta \\ \omega \end{bmatrix} + \underbrace{\begin{bmatrix} 0 \\ M^{-1} \end{bmatrix} T^{1/2}}_{B} \eta$$

where M, D, & T are diagonal & $L = L^{\mathsf{T}}$ (Laplacian)

Performance metric for emulation of rotational inertia



System norm quantifying signal amplifications

disturbances: impulse (fault), step (loss of unit), white noise (renewables) → system → **performance outputs:** integral, peak, ROCOF, restoration time, ...

Coherency performance metric & $\mathcal{H}_2$ norm

Energy expended by the system to return to synchronous operation:

$$\int_0^\infty \sum_{\{i,j\} \in \mathcal{E}} a_{ij}(\theta_i(t) - \theta_j(t))^2 + \sum_{i=1}^{n} s_i\, \omega_i^2(t)\, dt$$

$\mathcal{H}_2$ **system norm** interpretation: η → system → y

1. **performance output**: $\mathbf{y} = \begin{bmatrix} Q_1^{1/2} & 0 \\ 0 & Q_2^{1/2} \end{bmatrix} \begin{bmatrix} \theta \\ \omega \end{bmatrix}$
2. **impulsive** η (faults) $\longrightarrow$ output energy $\int_0^\infty \mathbf{y}(t)^{\mathsf{T}} \mathbf{y}(t)\, dt$
3. **white noise** η (renewables) $\longrightarrow$ output variance $\lim_{t \to \infty} \mathbb{E}\left(\mathbf{y}(t)^{\mathsf{T}} \mathbf{y}(t)\right)$

Algebraic characterization of the $\mathcal{H}_2$ norm

Lemma: $\mathcal{H}_2$ norm via observability Gramian

$$\|G\|_2^2 = \text{Trace}(B^{\mathsf{T}} P B)$$

where P is the observability Gramian $P = \int_0^\infty e^{A^{\mathsf{T}} t} Q e^{At}\, dt$

- P solves a Lyapunov equation: $P\,A + A^{\mathsf{T}} P + Q = 0$
- A has a zero eigenvalue $\rightarrow$ restricts choice of Q

$$y = \begin{bmatrix} Q_1^{1/2} & 0 \\ 0 & Q_2^{1/2} \end{bmatrix} \begin{bmatrix} \theta \\ \omega \end{bmatrix} \qquad Q_1^{1/2} \mathbb{1} = \mathbb{0}$$

- P is unique for $P\,[\mathbb{1}\ \mathbb{0}] = [\mathbb{0}\ \mathbb{0}]$

Problem formulation

$$\begin{aligned} \underset{P,\, m_i}{\text{minimize}} \quad & \text{Trace}(B^\top P B) && \rightarrow \text{performance metric} \\ \text{subject to} \quad & \textstyle\sum_{i=1}^{n} m_i \leq m_{\text{bdg}} && \rightarrow \text{budget constraint} \\ & \underline{m_i} \leq m_i \leq \overline{m_i}\,, \quad i \in \{1, \dots, n\} && \rightarrow \text{capacity constraint} \\ & P A + A^\top P + Q = 0 && \rightarrow \text{observability Gramian} \\ & P\,[\mathbb{1}\ \mathbb{0}] = [\mathbb{0}\ \mathbb{0}] && \rightarrow \text{uniqueness} \end{aligned}$$

Insights

1. m appears as m^{-1} in system matrices A, B
2. product of $B(m)$ & P in the objective
3. product of $A(m)$ & P in the constraint

$\Rightarrow$ **large-scale & non-convex**

optimal placement of virtual inertia

where would you place the inertia?

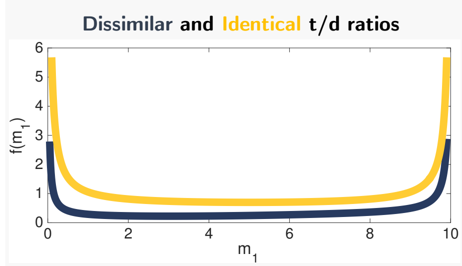
uniform, max capacity, near disturbance?

the more inertia the better?

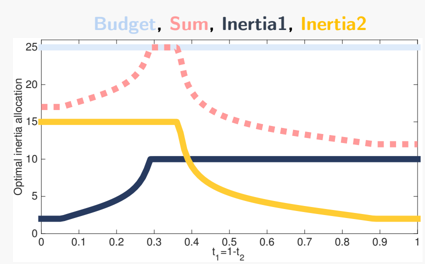
Building the intuition: results for two-area networks

Fundamental learnings

1. explicit closed-form solution is rational function
2. sufficiently uniform t_i/d_i $\rightarrow$ strongly **convex** & fairly **flat** cost
3. non trivial in the presence of capacity constraints



performance metric



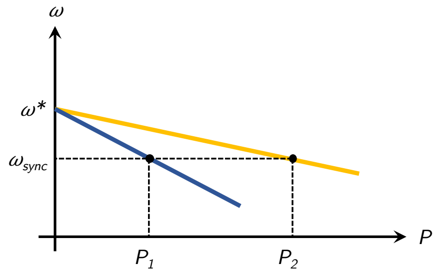
optimal inertia allocation

Closed-form results for cost of primary control

$P/\dot{\theta}$ primary droop control

$$(\omega_i - \omega^*) \propto (P_i^* - P_i(\theta))$$
$$\Updownarrow$$
$$D_i \dot{\theta}_i = P_i^* - P_i(\theta)$$

(can also model effect of PSS control)



Primary control effort → accounted for by integral quadratic cost

$$\int_0^\infty \dot{\theta}(t)^\top D\, \dot{\theta}(t)\, dt$$

which is the $\mathcal{H}_2$ performance for the penalties $Q_1^{1/2} = 0$ and $Q_2^{1/2} = D$

Primary control . . . cont'd

Theorem: the primary control effort optimization reads equivalently as

$$\begin{aligned} \underset{m_i}{\text{minimize}} \quad & \sum\nolimits_{i=1}^{n} \frac{t_i}{m_i} \\ \text{subject to} \quad & \sum\nolimits_{i=1}^{n} m_i \leq m_{\text{bdg}} \\ & \underline{m_i} \leq m_i \leq \overline{m_i}, \quad i \in \{1, \dots, n\} \end{aligned}$$

Key take-away is **disturbance matching**:

- optimal allocation $\propto \sqrt{t_i}$ or $m_i = \min\{m_{\text{bdg}}, \overline{m_i}\}$
- optimal allocation independent of network topology

Location & **strength** of disturbance are **crucial** solution ingredients

Robust inertia allocation

empirical disturbance distributions available but we want to prepare for "rare events"

$$\begin{aligned} \underset{P,\, m_i}{\text{minimize}}\ \underset{\mathbf{t_i}}{\textbf{maximize}} \quad & \text{Trace}(B(\mathbf{t_i^{1/2}})^\top P B(\mathbf{t_i^{1/2}})) & \rightarrow \textbf{robust performance} \\ \text{subject to} \quad & T \in \mathbb{T} & \rightarrow \textbf{disturbance family} \\ & t_i \geq 0\, \forall i \ \ \& \ \sum\nolimits_{i=1}^{n} t_i = 1 & \rightarrow \textbf{normalization} \end{aligned}$$

inertia budget, capacities, & Lyapunov equation

Key insights:

- inner maximization problem is **linear** in T

⇒ min - max can be converted to minimization by duality

- **valley filling** solution for primary control metric:

  $t_i^\star / m_i^\star = const.$ (up to constraints)

numerical method for the general case

Taylor & power series expansions

Key idea: scalar series expansion at m_i in direction μ_i:

$$\frac{1}{m_i + \delta\mu_i} = \frac{1}{m_i} - \frac{\delta\mu_i}{m_i^2} + \mathcal{O}(\delta^2)$$

⇒ expand system matrices via **Taylor series** in direction μ:

$$\mathbf{A}(m+\delta\mu) = A^{(0)}_{(m,\mu)} + A^{(1)}_{(m,\mu)}\delta + \mathcal{O}(\delta^2) \quad , \quad \mathbf{B}(m+\delta\mu) = \dots$$

⇒ expand observability Gramian via **power series** in direction μ:

$$\mathbf{P}(m+\delta\mu) = P^{(0)}_{(m,\mu)} + P^{(1)}_{(m,\mu)}\delta + \mathcal{O}(\delta^2)$$

Magic happens: the Lyapunov equation decouples

$$\mathbb{0} = \delta^0 \left(P^{(0)}A^{(0)} + A^{(0)\top}P^{(0)} + Q\right) + \delta^1 \left(P^{(1)}A^{(0)} + A^{(0)\top}P^{(1)} + \left(P^{(0)}A^{(1)} + A^{(1)\top}P^{(0)}\right)\right) + \mathcal{O}(\delta^2)$$

Explicit gradient computation

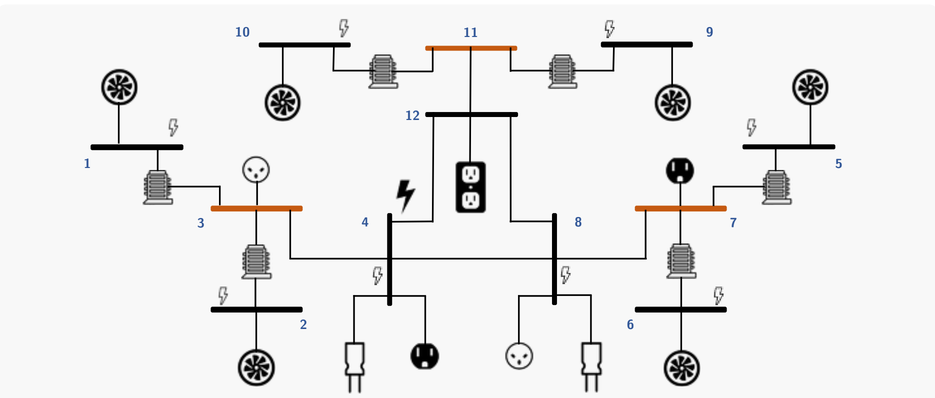
1. nominal Lyapunov equation for $\mathcal{O}(\delta^0)$:
   $$\mathbf{P^{(0)}} = \mathbf{Lyap}(\mathbf{A^{(0)}}, \mathbf{Q})$$
2. perturbed Lyapunov equation for $\mathcal{O}(\delta^1)$ terms:
   $$\mathbf{P^{(1)}} = \mathbf{Lyap}(\mathbf{A^{(0)}}, \mathbf{P^{(0)}A^{(1)}} + \mathbf{A^{(1)}}^\mathsf{T}\mathbf{P^{(0)}})$$
3. expand objective at m in direction μ:
   $$\text{Trace}(B(m)^\mathsf{T}\mathbf{P}(m)B(m)) = \text{Trace}((\dots) + \delta(\dots)) + \mathcal{O}(\delta^2)$$
4. gradient: $\text{Trace}(2 * B^{(1)\mathsf{T}}P^{(0)}B^{(0)} + B^{(0)\mathsf{T}}P^{(1)}B^{(0)})$

⇒ use favorite method for reduced optimization problem with explicit gradient & without Lyapunov constraint

results for a three-area case study

Modified Kundur case study: 3 areas & 12 buses

transformer reactance 0.15 p.u., line impedance (0.0001+0.001i) p.u./km



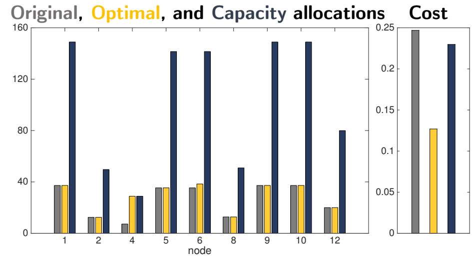
uniform deviation from sync as **performance metric**: $Q = \begin{bmatrix} I_n - \frac{1}{n}\mathbb{1}\mathbb{1}^T & \\ & I_n \end{bmatrix}$

Heuristics outperformed by $\mathcal{H}_2$ - optimal allocation

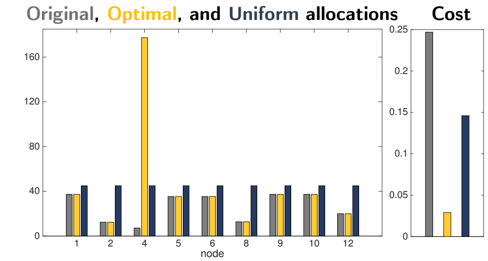
Scenario: disturbance at #4

- locally optimal solution **outperforms heuristic** max/uniform allocation
- optimal allocation ≈ **matches disturbance**
- inertia emulation at all undisturbed nodes is actually **detrimental**

$\Rightarrow$ **location** of disturbance & inertia emulation matters

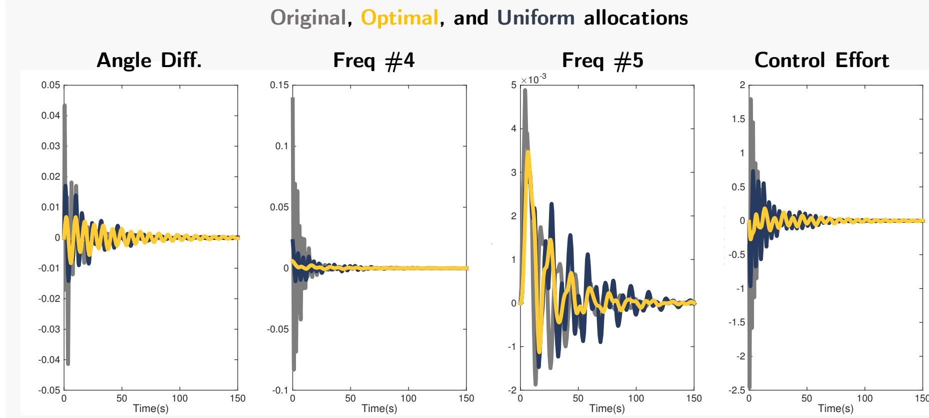


allocation subject to capacity constraints



allocation subject to the budget constraint

Eye candy: time-domain plots of post fault behavior



Take-home messages:

best oscillation performance	smallest peak frequency at #4	undisturbed sites are irrelevant	minimal control effort $m_i \cdot \ddot{\theta}_i$

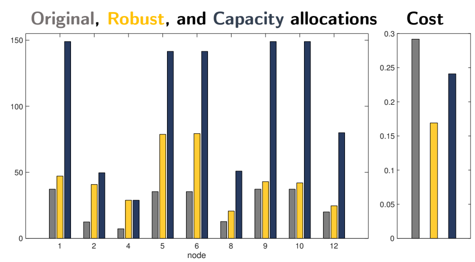
Robust min - max allocation

Scenario: fault (impulse) can occur at any single node

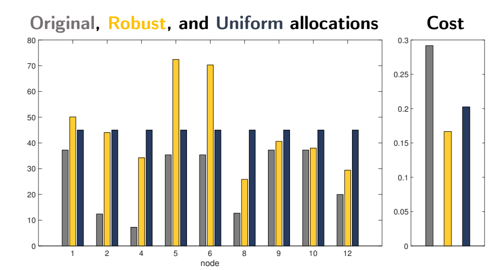
- disturbance set $T \in \mathbb{T} = \{\mathbb{e}_1 \cup \cdots \cup \mathbb{e}_{12}\}$

$\Rightarrow$ min / max over convex hull

- robust inertia allocation **outperforms** heuristics
- results become **more intuitive**: the more inertia (capacity & budget) the better & valley-filling property



allocation subject to capacity constraints



allocation subject to the budget constraint

conclusions

Conclusions

Where to do it?

1. $\mathcal{H}_2$-optimal (non-convex) allocation
2. closed-form results for cost of primary control
3. numerical approach via gradient computation

How to do it?

1. down-sides of naive inertia emulation
2. novel machine matching control

What else to do? Inertia emulation is . . .

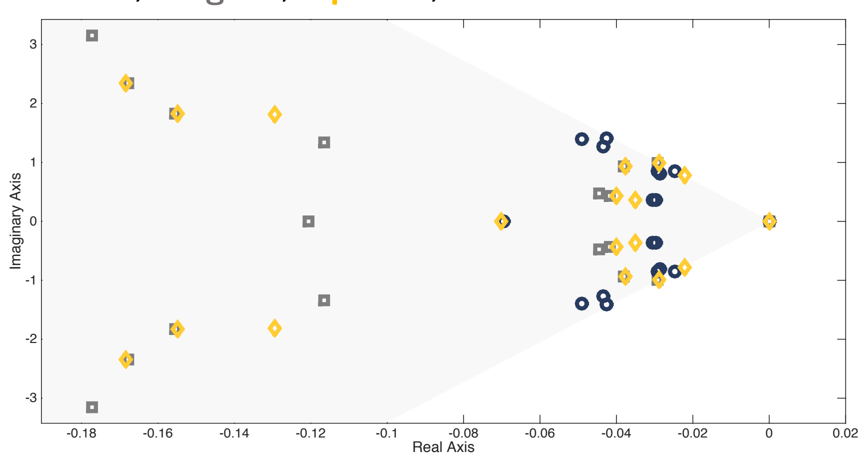
☺ decentralized, plug'n'play (passive), grid-friendly, user-friendly, . . .

☹ suboptimal, wasteful in control effort, & need for new actuators

appendix

Spectral perspective on different inertia allocations

Cone, Original, Optimal, and Uniform allocations



- $\mathbf{m} = \underline{\mathbf{m}}$ → best damping asymptote & best damping ratio
- spectrum holds only **partial information !!**

The planning problem

sparse allocation of limited resources

ℓ_1-regularized inertia allocation (promoting a sparse solution):

$$\begin{aligned}
\underset{P\,,\,m_i}{\text{minimize}} \quad & \mathbf{J}_\gamma(\mathbf{m},\mathbf{P}) = \|G\|_2^2 + \gamma\|\mathbf{m} - \underline{\mathbf{m}}\|_1 \\
\text{subject to} \quad & \textstyle\sum_{i=1}^{n} m_i \le m_{\text{bdg}} \\
& \underline{m_i} \le m_i \le \overline{m_i} \quad i \in \{1,\dots,n\} \\
& P\,A + A^{\mathsf{T}} P + Q = 0 \\
& P[\mathbb{1}\ \mathbb{0}] = [\mathbb{0}\ \mathbb{0}]
\end{aligned}$$

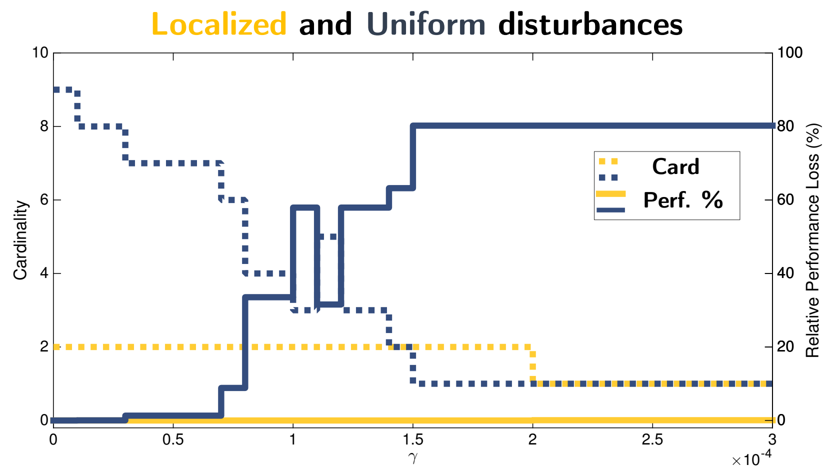
where $\gamma \ge 0$ trades off sparsity penalty and the original objective

Highlights:

1. regularization term is linear & **differentiable**
2. gradient computation algorithm can be used with some tweaking

Relative performance loss (%) as a function of γ

0% $\rightarrow$ optimal allocation, **100%** $\rightarrow$ no additional allocation



1. uniform disturbance $\Rightarrow \exists\, \gamma$ **1.3%** loss $\equiv$ **(9 $\rightarrow$ 7)**
2. localized disturbance $\Rightarrow$ **(2 $\rightarrow$ 1)** without affecting performance

Uniform disturbance to damping ratio

power sharing $\rightarrow$ $\mathbf{d} \propto P^*$, assuming $\mathbf{t} \propto$ source rating P^*

Theorem: for $t_i/d_i = t_j/d_j$ the allocation problem reads equivalently as

$$\begin{array}{ll} \underset{m_i}{\text{minimize}} & \sum_{i=1}^{n} \frac{s_i}{m_i} \\ \text{subject to} & \sum_{i=1}^{n} m_i \le m_{\text{bdg}} \\ & \underline{m_i} \le m_i \le \overline{m_i}, \quad i \in \{1, \ldots, n\} \end{array}$$

Key takeaways:

- optimal solution independent of network topology
- allocation $\propto \sqrt{s_i}$ or $m_i = \min\{m_{\text{bdg}}, \overline{m_i}\}$

What if **freq. penalty $\propto$ inertia**? $\rightarrow$ norm **independent** of inertia

Taylor & power series expansions

Key idea: expand the performance metric as a power series in m

$$\|G\|_2^2 = \text{Trace}(B(m)^{\mathsf{T}} \mathbf{P}(\mathbf{m}) B(m))$$

Motivation: scalar series expansion at m_i in direction μ_i:

$$\frac{1}{(m_i + \delta \mu_i)} = \frac{1}{m_i} - \frac{\delta \mu_i}{m_i^2} + \mathcal{O}(\delta^2)$$

Expand system matrices in direction μ, where $\Phi = \text{diag}(\mu)$:

$$\mathbf{A}^{(0)}_{(\mathbf{m},\mu)} = \begin{bmatrix} 0 & I \\ -M^{-1}L & -M^{-1}D \end{bmatrix}, \quad \mathbf{A}^{(1)}_{(\mathbf{m},\mu)} = \begin{bmatrix} 0 & 0 \\ \Phi M^{-2} L & \Phi M^{-2} D \end{bmatrix}$$

$$\mathbf{B}^{(0)}_{(\mathbf{m},\mu)} = \begin{bmatrix} 0 \\ M^{-1} T^{1/2} \end{bmatrix}, \quad \mathbf{B}^{(1)}_{(\mathbf{m},\mu)} = \begin{bmatrix} 0 \\ -\Phi M^{-2} T^{1/2} \end{bmatrix}$$

Taylor & power series expansions cont'd

Expand the observability Gramian as a power series in direction μ

$$\mathbf{P}(m) = \mathbf{P}(m + \delta\mu) = \mathbf{P}^{(0)}_{(m,\mu)} + \mathbf{P}^{(1)}_{(m,\mu)} \delta + \mathcal{O}(\delta^2)$$

Formula for gradient in direction μ

1. nominal Lyapunov equation for $\mathcal{O}(\delta^0)$: $\mathbf{P}^{(0)} = \mathbf{Lyap}(\mathbf{A}^{(0)}, \mathbf{Q})$
2. perturbed Lyapunov equation for $\mathcal{O}(\delta^1)$ terms:

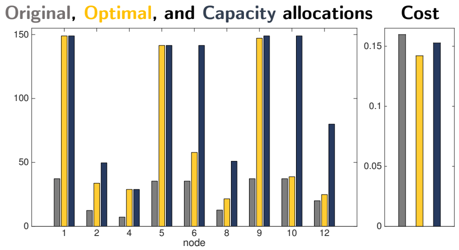
$$\mathbf{P}^{(1)} = \mathbf{Lyap}(\mathbf{A}^{(0)}, \mathbf{P}^{(0)} \mathbf{A}^{(1)} + \mathbf{A}^{(1)\mathsf{T}} \mathbf{P}^{(0)})$$

3. expand objective in direction μ:

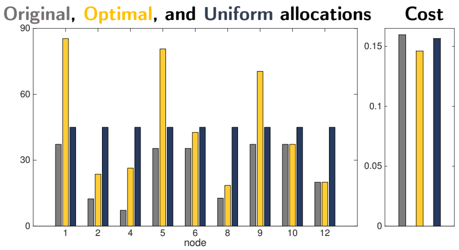
$$\|G\|_2^2 = \text{Trace}(B(m)^{\mathsf{T}} \mathbf{P}(m) B(m)) = \text{Trace}((\ldots) + \delta(\ldots)) + \mathcal{O}(\delta^2)$$

4. gradient: $\mathbf{Trace}(2 * \mathbf{B}^{(1)\mathsf{T}} \mathbf{P}^{(0)} \mathbf{B}^{(0)} + \mathbf{B}^{(0)\mathsf{T}} \mathbf{P}^{(1)} \mathbf{B}^{(0)})$

Heuristics outperformed also for uniform disturbance



allocation subject to capacity constraints



allocation subject to the budget constraint

Scenario: uniform disturbance

Heuristics for placement:

1. **max** allocation in case of capacity constraints
2. **uniform** allocation in case of budget constraint

Results & insights:

1. locally optimal solution **outperforms** heuristics
2. optimal solution $\neq$ **max** inertia at each bus